

Design And Analysis Of Stirling Engine For Underwater Application

Rajkumar Bhagat¹, Harsh Khandelwal², Shreyash Khandwe³, Akshay Khubchandani⁴, Kanhaiya Kuche⁵, Sohan Kulal⁶, Utkarsha Chinde⁷

¹Faculty, Vishwakarma Institute of Technology, Pune, Maharashtra, India

²⁻⁷ B. Tech, Mechanical Department, Vishwakarma Institute of Technology, Pune, Maharashtra, India

Abstract - Selection of power systems for underwater vehicles is an important task. The power system must be compact enough to fit inside the vehicle and it should supply sufficient power. *This paper presents thermodynamic analysis of the Stirling engine based on schmidt analysis for underwater application. Alpha type engine with opposed cylinder configuration is selected. After the analysis, Dimensions for each component are selected followed by structural analysis of engine components.*

Key Words: Stirling Engine, thermodynamic analysis, underwater application, cooler, Regenerator, Unmanned vehicle.

1. INTRODUCTION

Stirling Engine is a closed cycle heat engine in which no external air is required which makes it ideal for underwater application. The silent operation of it makes the vehicle more stealthy which makes the engine attractive for military applications. In the 2005 war games, USS *Ronald Reagan*, a newly constructed \$6.2 billion dollar aircraft carrier, was sunk after being hit by multiple torpedoes. This torpedo was launched by Sweden's submarine named "Gotland". Gotland snuck past us ronald reagan defenses. Americans never saw it coming and Yet despite making multiple attack runs on the *Reagan*, never saw it leave. Previously, diesel submarines could only navigate with noisy diesel engines powered by air and stay underwater for a few days. As a result, diesel submarines were most vulnerable while snorkeling and could be easily tracked. On the other hand, submarines fueled by nuclear reactors require large amounts of coolant to prevent a meltdown. Hence pumping of coolant creates noises and vibrations which can be easily detected by SONAR. The Swedish Gotlands uses a 75 KW stirling engine which is an External combustion engine. Therefore frequent combustion does not take place while operation and there is gradual compression and expansion of working gas which makes it more silent.

Stirling Engines can be used for the underwater vehicles that can operate underwater with or without a human

occupant. They can be used for surveillance and other missions that require very quiet operation. A closed-cycle heat engine has potentially better overall energy density than available battery systems. For example, 100 mile range, Submersible with 2m Diameter and 10m Length operating at 10 Knots for 1 hour requires 200 KW-Hr of energy. If we use a 35W-hr/Kg lead acid battery, We would require 6 tons of it. Above requirement can be fulfilled by the 15 kW, 100 kg stirling engine. Although the weight of the reactant storage must be added to this, the total propulsion package with a Stirling could be lighter than the propulsion package with advanced batteries.

Among Alpha, Beta, Gamma type stirling engines, Alpha type is more efficient and has more power density. So that, Alpha type stirling engine with opposed cylinder configuration is designed. In this type of configuration, Instead of displacer, Two separate cylinders are used. One is connected to the heater and the other is connected to the cooler. Regenerator between heater and cooler acts as a heat reservoir.

1.1 Aim Of The Work

The purpose of this article is to design the Stirling engine and its various components as well as the analysis of the engine (strain, stress, deformation). Theoretical thermodynamic analysis was also performed for the engine.

2. METHODOLOGY

Work took place in three stages, first the Stirling engine was modeled by Schmidt analysis using ratings taken from various references. Then it was modeled and then partially imported in analysis software where structural analysis is performed.

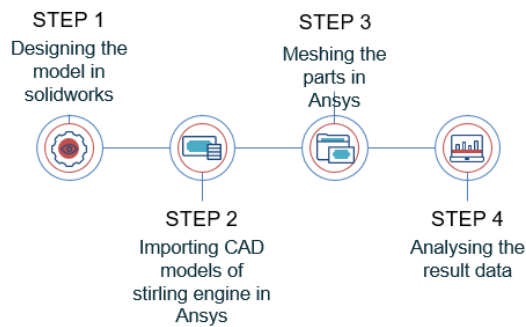


Fig -1: Mind Map

2.1 Theoretical Analysis

Opposite cylinder configuration type is selected for the design for the optimum use of volume inside the vehicle. Schmidt's analysis is used to model the system. This analysis is still used today as the classical analysis of the Stirling cycle.

Following are the assumptions for this analysis:

- working fluid obeys ideal gas law
- Engine is perfectly sealed and there is no working fluid leakage. Thus total mass of working fluid is constant
- Temperature in each working space (compression, Expansion) is known and there is no temperature gradient
- Engine is running at constant speed
- Uniform instantaneous pressure in the working space

Following are some of the parameters selected for the engine:

Stroke = 60mm
 Crank radius (r) = 30mm
 Clearance length = 4 mm
 Bore Diameter (D) = 52.4 mm
 $T_c = 350K$
 $T_h = 923 K$
 $n = 1200 \text{ rpm}$

$V_{\text{regen}} = 154 \text{ cm}^3$
 $D_{\text{regen}} = 60 \text{ mm}$
 $L_{\text{regen}} = 4 V_{\text{regen}} / \pi D_{\text{regen}}^2$
 $L_{\text{regen}} = 54.46\text{mm}$

Now, Let's find out variation of working volumes with crank angles

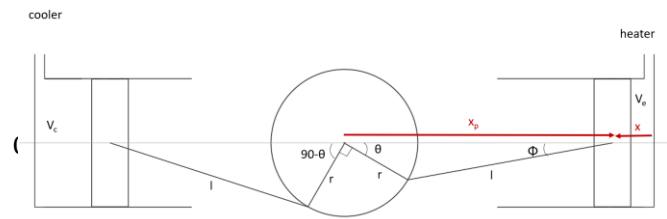


Fig -2: Engine system Configuration

$$x_p = r \cos(\theta) + l \cos(\phi)$$

$$\sin\phi = r \sin\theta / l$$

$$\cos\phi = \frac{\sqrt{n^2 - \sin^2\theta}}{n}$$

$$x = r(1 - \cos\theta) + r(n - \sqrt{n^2 - \sin^2\theta})$$

$$V_e = \frac{\pi}{4} D^2 r (1 - \cos\theta) + r(n - \sqrt{n^2 - \sin^2\theta})$$

Similarly, we can find out variation of compression volume with crank angle

$$V_c = \frac{\pi}{4} D^2 r (1 - \sin\theta) + r(n - \sqrt{n^2 - \cos^2\theta})$$

Mass of the gas

$$M = (P_{\text{atm}} V_{\text{total (max)}}) \div (R T_{\text{initial}})$$

Where,

$P_{\text{atm}} = 101325 \text{ N/m}^2$
 $V_{\text{total (max)}} = 372.63 \text{ cm}^3$
 $T_{\text{initial}} = 293.15 \text{ k}$
 $R = 287 \text{ J/kg-k}$

$$M = 0.4375 \text{ g}$$

$$M_{\text{total}} = M_e + M_c + M_{\text{regen}}$$

$$M_{\text{total}} = P/R (V_e / T_e + V_r / T_r + V_c / T_c)$$

$$P = M_{\text{total}} R / (V_e / T_e + V_r / T_r + V_c / T_c)$$

$$T_r = (T_h - T_c) / \ln(T_h / T_c)$$

$$T_r = 590.9 \text{ K}$$

2.2 Flywheel Design

Torque developed by expansion piston on crank will be given by-

$$T_e = r F_p [\sin\theta + \sin(2\theta) / 2 \sqrt{(n^2 - \sin^2\theta)}]$$

Where,

$$F_p = \pi/4 D^2 P$$

Torque developed by compression piston on crank will be given by-

$$T_c = r F_p [\cos\theta + \sin(2\theta) / 2 \sqrt{(n^2 - \cos^2\theta)}]$$

$$\text{Total torque (T)} = T_e + T_c$$

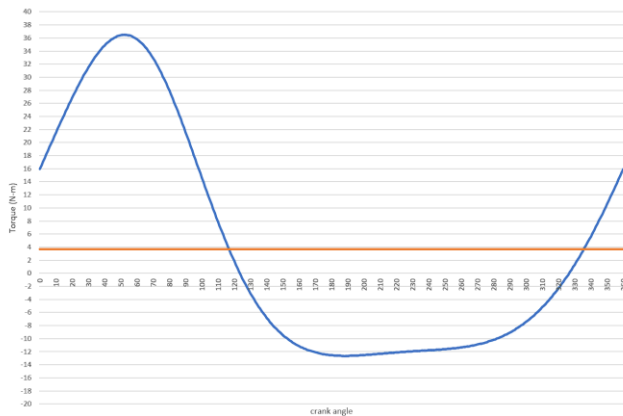


Chart -1: Turning moment diagram

Work developed by the engine = work require for an application

$$\text{Area of turning moment diagram} = T_{\text{mean}} 2\pi$$

$$T_{\text{mean}} = \text{Area of turning moment diagram} / 2\pi$$

$$T_{\text{mean}} = 22.88 / 2\pi = 3.64 \text{ Nm}$$

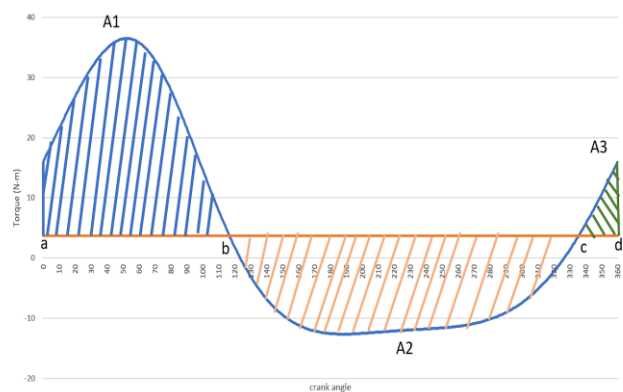


Chart -2: Turning Moment with Area

$$A1 = 45 \text{ Nm}$$

$$A2 = 46.85 \text{ Nm}$$

$$A3 = 2.5 \text{ Nm}$$

Let energy at point a be E

$$A : E$$

$$b : E + A1$$

$$c : E + A1 - A2$$

$$d : E + A1 - A2 + A3 = E$$

Maximum fluctuation of energy -

$$\Delta E = \text{maximum energy} - \text{Minimum energy}$$

$$\Delta E = \text{energy at b} - \text{energy at c}$$

$$\Delta E = (E + A1) - (E + A1 - A2)$$

$$\Delta E = A2 = 46.85 \text{ Nm}$$

Coefficient of fluctuation of speed (C_s) = 0.03

Solid disk type flywheel is selected

$$\text{Maximum fluctuation of energy in flywheel} = \frac{1}{2} I \omega^2 C_s$$

$$\Delta E = \frac{1}{2} I \omega^2 C_s$$

Where,

$$\omega = 2\pi n / 60 = 125.66 \text{ rad/s}$$

$$I = 0.098 \text{ Kg-m}^2$$

$$I = M (R_o^2 - R_i^2) / 2$$

$$M = \rho \pi (R_o^2 - R_i^2) t$$

$$I = \rho \pi (R_o^2 - R_i^2)^2 t / 2$$

$$\rho = 7800 \text{ kg/m}^3 \text{ (carbon steel)}$$

$$R_i = \text{shaft radius} = 10 \text{ mm}$$

$$t = 10 \text{ mm}$$

$$R_o = 31.53 \text{ mm}$$

2.3 Cooler

For cooler, Equivalent model was designed using ansys and the analysis is carried out. Taking the regenerator temperature as the inlet, We must achieve the temperature of 350K. The surface area is calculated which can produce that much temperature difference. Following parameters are taken for the analysis:

Table -1: Specifications

Parameters	Specifications
Cooler temperature	20-30°C, Average : 25°C
Heater temperature	923K=650°C
Heating method	liquid oxygen and diesel to create the heating of the engine in the

	combustion chamber.
Cooling method	cold seawater
material	copper
tube diameter	300 mm
shell diameter	1000 mm
length	4000 mm

It was observed that surface area of 0.2827 m² is sufficient to produce the temperature difference

2.4 CAD Modelling

Piston

The pistons of the Stirling engine are hermetically sealed and are driven to move up and down as the gas inside expands. We use gray cast iron material for piston.

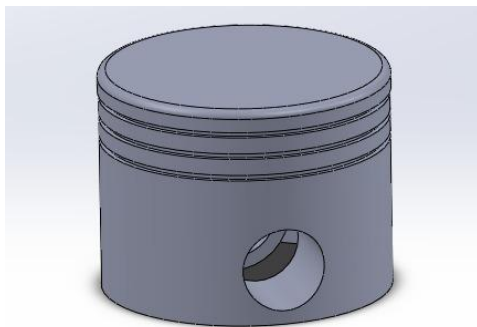


Fig -2: Piston CAD Model

Connecting Rod

A device used to connect two moving parts, where it is used between the crankshaft and the piston. Here we have used carbon steel material for it.



Fig -3: Connecting Rod CAD Model

Flywheel

The design of the flywheel is done in the previous section. It is used to minimize the fluctuations in the output power. Carbon steel is used as a material

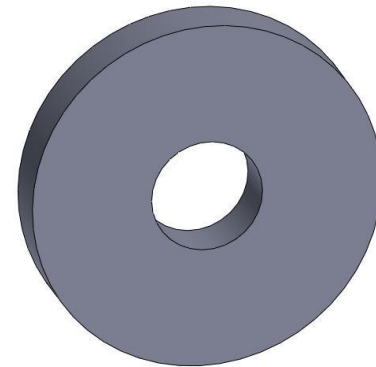


Fig -4: Flywheel CAD Model

Gudgeon pin

The Gudgeon/piston pin is used to connect the piston to the connecting rod. It also provides a bearing on which the connecting rod rotates as the piston moves.

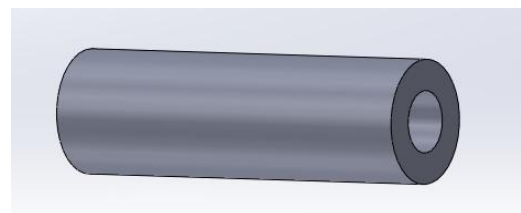


Fig -5: Gudgeon Pin CAD Model

Regenerator

In a Stirling engine, the regenerative is an internal heat exchanger and a heat reservoir temporarily placed between the hot and cold spaces so that the working fluid passes through it first in one direction and then in the other. Its function is to retain in the system heat that would otherwise be exchanged with the intermediate temperature medium at the maximum and minimum cycle temperatures. Copper is used as a material.



Fig -6: Regenerator CAD Model

Engine housing

An engine house is a structure that holds the moving parts.

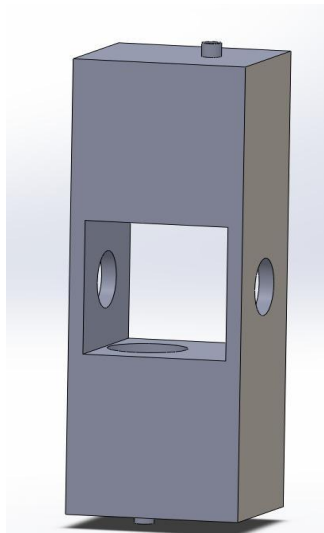


Fig -7: Engine housing CAD Model

Spur Gear

Spur/Cylindrical gears are used in mechanical applications to increase or decrease the speed of equipment or multiply torque by transmitting motion and power via a belt drive.

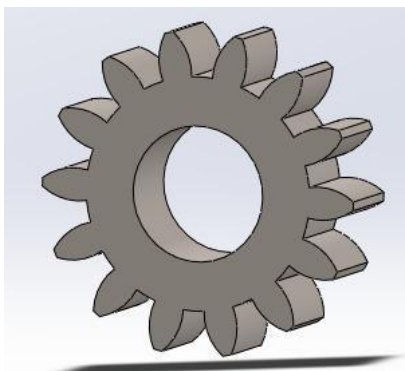


Fig -8: Spur gear CAD Model

Crankshaft

The shaft through which the mechanical work is transferred from the piston to the flywheel.

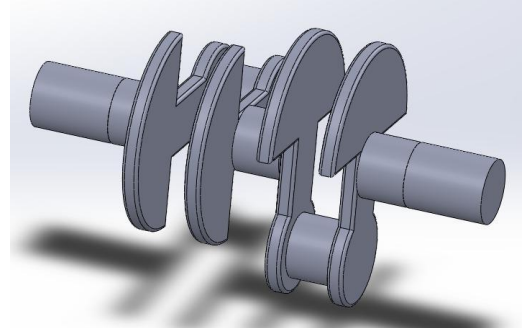


Fig -9: Crankshaft CAD Model

Bearing

A bearing is a part of machinery that limits motion relative to only the desired motion and reduces friction between moving parts.

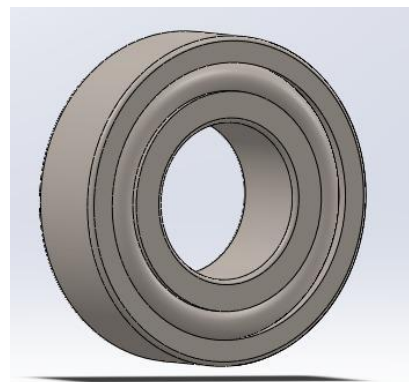


Fig -10: Bearing CAD Model

Pipe

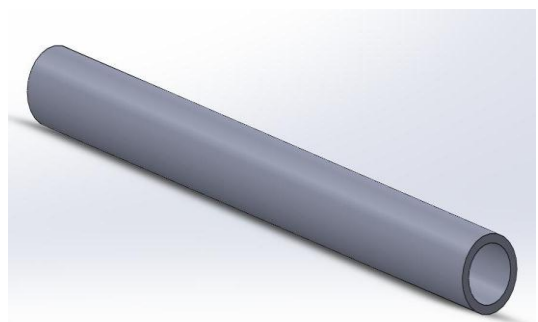


Fig -11: Pipe CAD Model

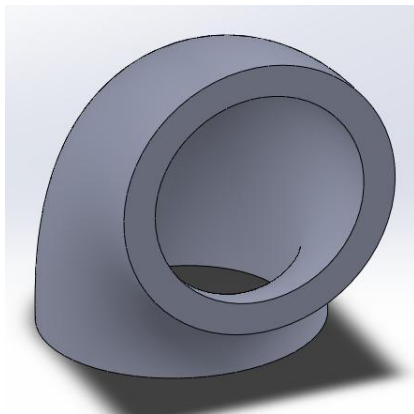


Fig -12: Pipe bend CAD Model

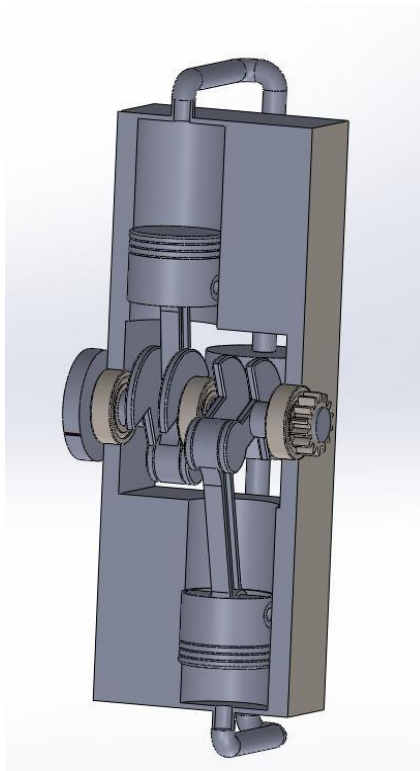


Fig -13: Assembly Section View

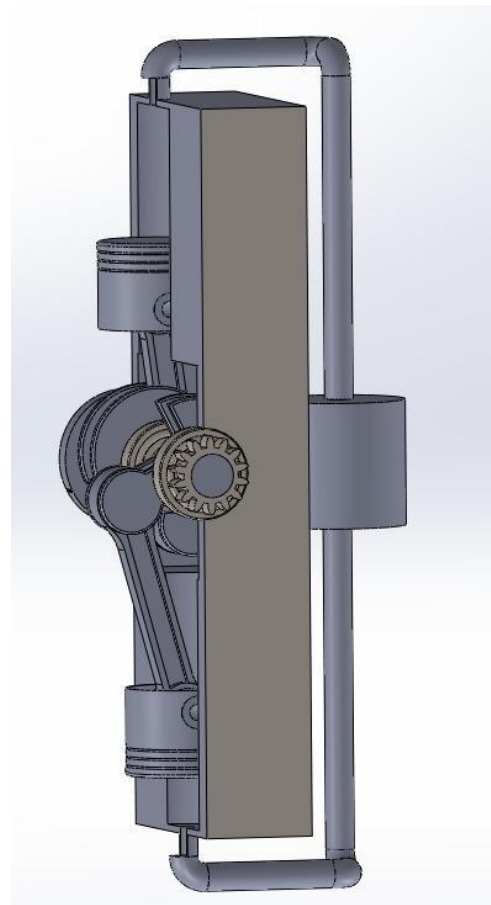


Fig -14: Assembly side view

3. RESULT

3.1 Theoretical Thermodynamic Results

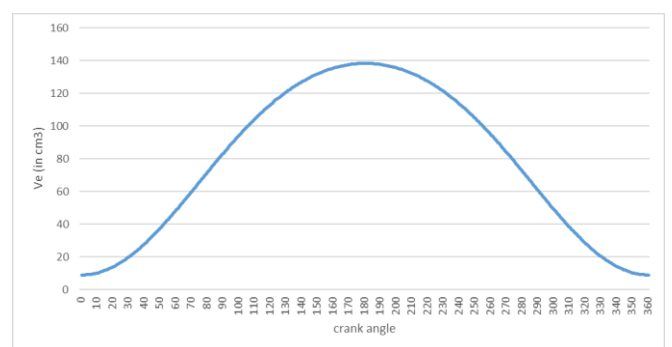


Chart -3: Variation of Expansion Volume with Crank Angle

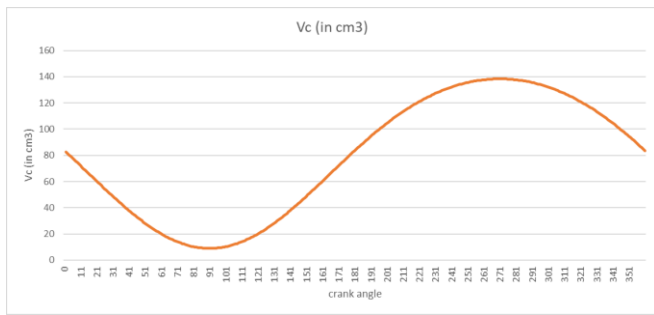


Chart -4: Variation of Compression Volume with Crank Angle

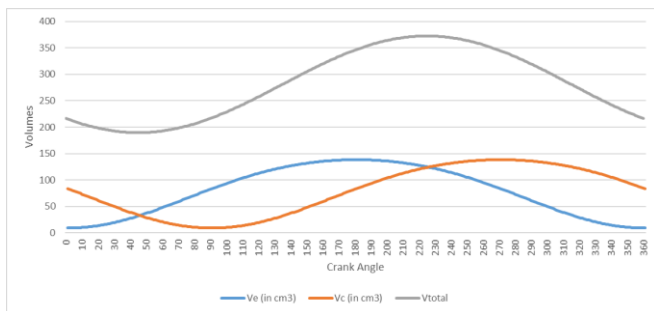


Chart -5: Variation of Total Volume with Crank Angle

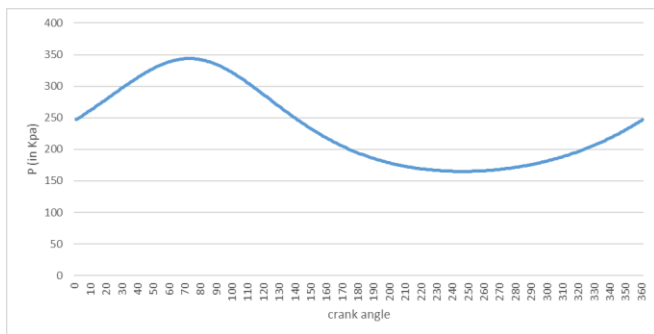


Chart -6: Variation of Pressure with Crank Angle

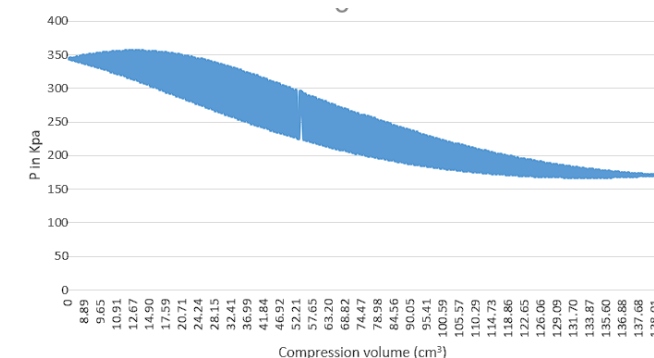


Chart -7: Variation of Pressure with Compression Volume

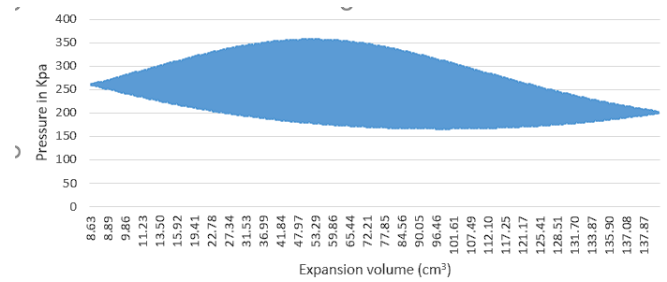


Chart -8: Variation of Pressure with Expansion Volume

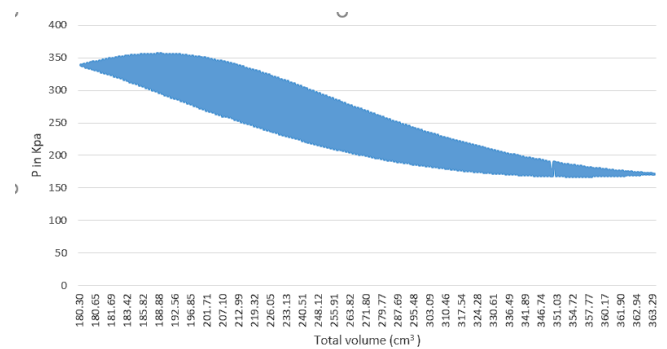


Chart -9: Variation of Pressure with Total Volume

3.2 Structural Analysis

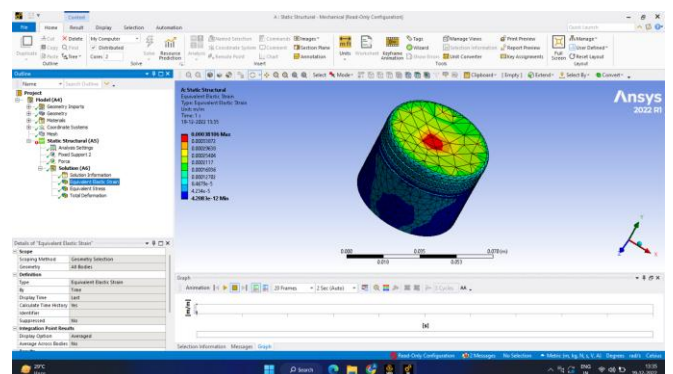


Fig -15: Piston - Equivalent Elastic Strain

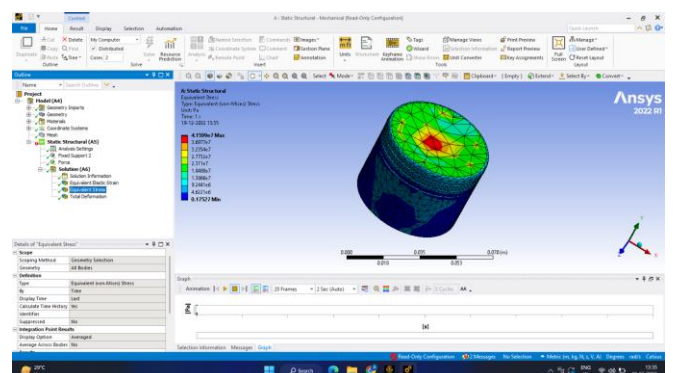


Fig -16: Piston - Equivalent stress

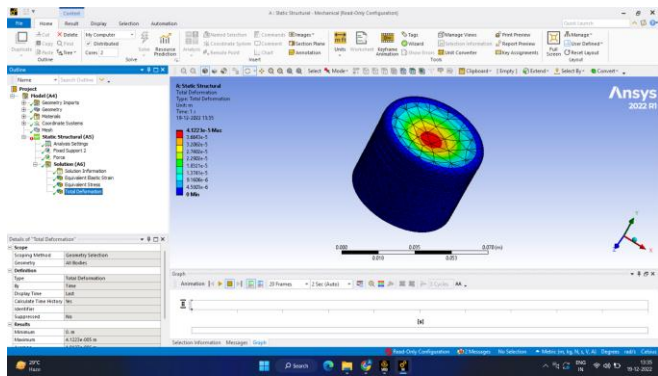


Fig -17: Piston - Total Deformation

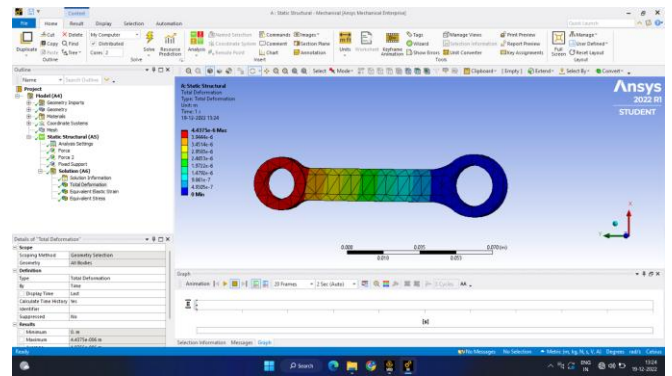


Fig -21: Connecting Rod - Total Deformation

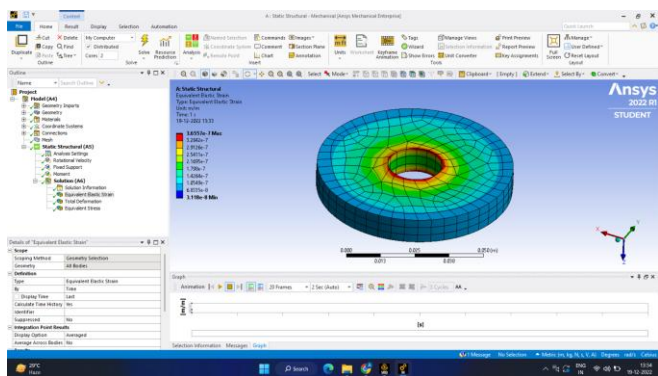


Fig -18: Flywheel- Equivalent Elastic Strain

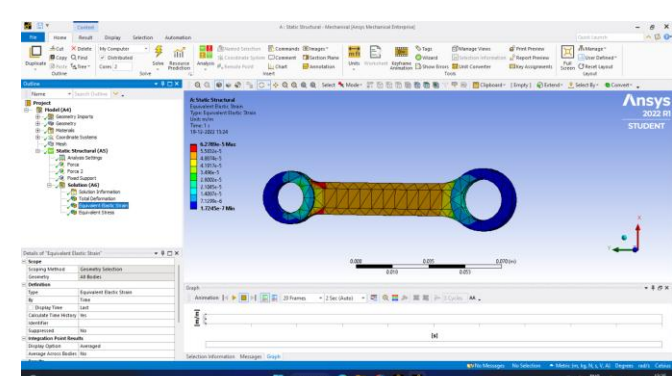


Fig -22: Connecting Rod - Equivalent Elastic Strain

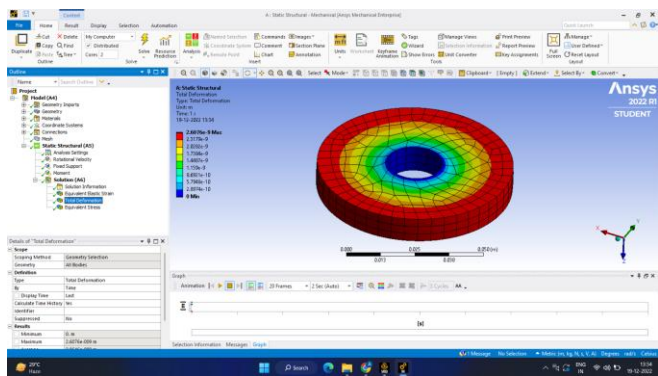


Fig -19: Flywheel- Total Deformation

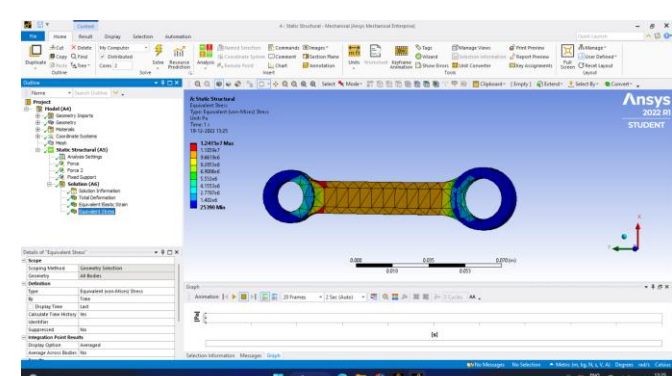


Fig -23: Connecting Rod - Equivalent stress

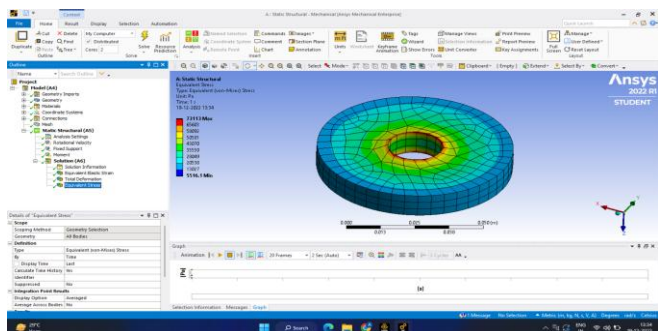


Fig -20: Flywheel- Equivalent stress

3.3 CFD Analysis

The equivalent model was used to determine the surface area required to achieve the required temperature difference. The surface is found to be 0.2827 m².

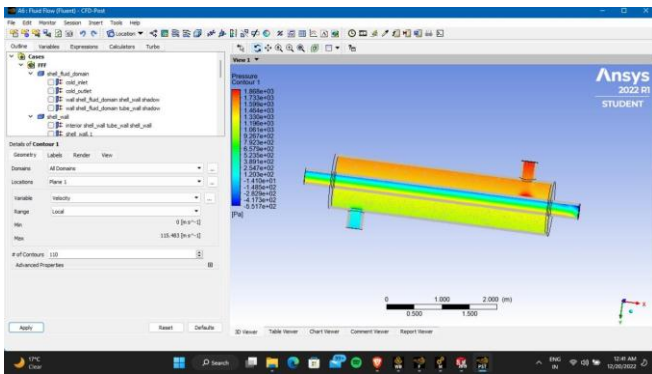


Fig -24: Pressure Contour

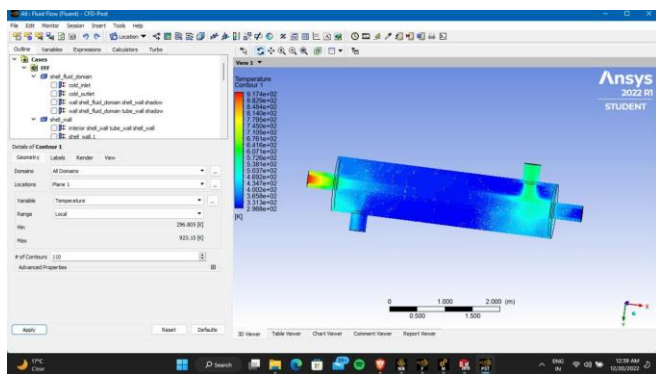


Fig -25: Temperature Contour

4. CONCLUSION

By doing the thermodynamic analysis, It is concluded that work done for compression is smaller than work obtained in the expansion stroke. So that net work of 10.735 Joule is obtained. considering 1200 rpm speed, cycle completed in 1 second will be 20 hence power obtained is 214.7 Watts. Structural analysis is done in ansys and the deformation, Von mises stress, strain is calculated. Stress induced in the piston was 41 Mpa and 21 Mpa for the connecting rod which are well within the permissible limits.

5. FUTURE SCOPE

Effect of pressure drop due to friction can be taken into consideration to correctly model thermodynamic analysis Working fluid like helium can be used for the efficient operation due to its high conduction coefficient and low drag coefficient.

REFERENCES

[1] Reader, Graham Thomas. "Stirling engines." (1983).

[2] Hargreaves, Clifford M. "The Phillips Stirling engine." (1991).

[3] Martini, William R. Stirling engine design manual. No. NASA-CR-168088. 1983.

[4] Organ, Allan J. "The regenerator and the Stirling engine." (1997).

[5] Walker, Graham. "Stirling engines." (1980).

[6] Sripakagorn, A. and Srikam, C., 2011. Design and performance of a moderate temperature difference Stirling engine. *Renewable Energy*, 36(6), pp.1728-1733.

[7] Urieli, Israel, and David M. Berchowitz. "Stirling cycle engine analysis." (1984).

[8] Ahmadi, Mohammad H., Mohammad-Ali Ahmadi, and Fathollah Pourfayaz. "Thermal models for analysis of performance of Stirling engine: A review." *Renewable and Sustainable Energy Reviews* 68 (2017): 168-184.

[9] Costea, M., S. Petrescu, and C. Harman. "The effect of irreversibilities on solar Stirling engine cycle performance." *Energy conversion and management* 40, no. 15-16 (1999): 1723-1731.

[10] Chen, N. C. J., and F. P. Griffin. Review of Stirling-engine mathematical models. No. ORNL/CON-135. Oak Ridge National Lab., TN (USA), 1983.

[11] Singh, Uday Raj, and Anil Kumar. "Review on solar Stirling engine: Development and performance." *Thermal Science and Engineering Progress* 8 (2018): 244-256.

[12] Campos, M. C., J. V. C. Vargas, and J. C. Ordonez. "Thermodynamic optimization of a Stirling engine." *Energy* 44, no. 1 (2012): 902-910.

[13] Paul, Christopher J., and Abraham Engeda. "Modeling a complete Stirling engine." *Energy* 80 (2015): 85-97.

[14] Scollo, L. S., P. E. Valdez, S. R. Santamarina, M. R. Chini, and J. H. Baron. "Twin cylinder alpha Stirling engine combined model and prototype redesign." *International journal of hydrogen energy* 38, no. 4 (2013): 1988-1996.

[15] Almajiri, Ahmad K., Saad Mahmoud, and Raya Al-Dadah. "Modeling and parametric study of an efficient Alpha type Stirling engine performance based on 3D CFD analysis." *Energy conversion and management* 145 (2017): 93-106.

- [16] Altin, Murat, Melih Okur, Duygu Ipci, Serdar Halis, and Halit Karabulut. "Thermodynamic and dynamic analysis of an alpha type Stirling engine with Scotch Yoke mechanism." *Energy* 148 (2018): 855-865.
- [17] Tlili, I. A. "Numerical investigation of an Alpha Stirling engine using the Ross Yoke linkage." *Heat Technol* 30 (2012): 23-36.
- [18] Boretti, Alberto. " α -Stirling hydrogen engines for concentrated solar power." *International Journal of Hydrogen Energy* 46, no. 29 (2021): 16241-16247.
- [19] Zare, Shahryar, and AliReza Tavakolpour-Saleh. "Free piston Stirling engines: A review." *International Journal of Energy Research* 44, no. 7 (2020): 5039-5070.
- [20] Alberti, Fabrizio, and Luigi Crema. "Design of a new medium-temperature Stirling engine for distributed cogeneration applications." *Energy Procedia* 57 (2014): 321-330.
- [21] Brett, C. "The 4-95 Stirling engine for underwater application." In *Proceedings of the 25th Intersociety Energy Conversion Engineering Conference*, vol. 5, pp. 530-533. IEEE, 1990.
- [22] Reader, Graham T., Ian J. Potter, Eric J. Clavelle, and Owen R. Fauvel. "Low power Stirling engine for underwater vehicle applications." In *Proceedings of 1998 International Symposium on Underwater Technology*, pp. 411-416. IEEE, 1998.
- [23] Potter, Ian J., and Graham T. Reader. *Operational feasibility of underwater Stirling engine systems using oxygen-seawater extraction*. No. CONF-950729-. American Society of Mechanical Engineers, New York, NY (United States), 1995.
- [24] Reader, G. T., and I. J. Potter. "Stirling machine technology for subsea intervention." In *The Ninth International Offshore and Polar Engineering Conference*. OnePetro, 1999.
- [25] Aoki, Taro, Satoshi Tsukioka, Takashi Murashima, Hiroshi Yoshida, Hidehiko Nakajoh, Tadahiro Hyakudome, Shoujirou Ishibashi, and Ryoko Sasamoto. "Deep Sea Unmanned Underwater Vehicles in JAMSTEC." In *The Thirteenth International Offshore and Polar Engineering Conference*. OnePetro, 2003.
- [26] Oelrich, Ivan C., and Frederick R. Riddell. *Evaluation of Potential Military Applications of Stirling Engines*. INSTITUTE FOR DEFENSE ANALYSES ALEXANDRIA VA, 1988.
- [27] FIJALKOWSKI, BOGDAN THADDEUS. "Unmanned Submarines (US) for Noiseless Naval Hazardous-Duty Missions."
- [28] Li, Daijin, Kan Qin, and Kai Luo. "Underwater stirling engine design with modified one-dimensional model." *International Journal of Naval Architecture and Ocean Engineering* 7, no. 3 (2015): 526-539.
- [29] Friedman, Norman. "Submarines-the future." *Asia-Pacific Defence Reporter* (2002) 36, no. 10 (2010).
- [30] Reader, G. T., J. Potter, and J. G. Hawley. "The evolution of AUV power systems." In *OCEANS 02 MTS/IEEE*, vol. 1, pp. 191-198. IEEE, 2002.
- [31] Bratt, Christer, and Hans-Goran Nelving. "Development and production of Stirling engines for submarine and solar application at Kockums." (2000).