

Comprehensive Geometric and Pavement Design of Kabaya Road, Rwanda

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Abstract:- The objective of the project was to conduct geometrical and pavement design of road located in Ngororero district, country of Rwanda and for achieving the intended objective, the raw data of the study were collected first by conducting topographic survey which helped to get both safe horizontal and vertical alignment. Secondly, different soil tests like CBR was conducted to determine the thickness of subbase layer, modified proctor was conducted to predict the optimum moisture content and maximum dry density respectively required during compaction on the field, Atterberg limits were conducted to know the plasticity of the soil mass and sieve analysis test was performed to know the soil contents and their behavior under applied load. Thirdly, the traffic survey was conducted in order to know the thickness of road base plus surfacing layer. The work was completed in Cavadis for the side of Auto-CAD, Autopiste, and Piste for geometric design and then after in Arc GIS for rendering works. Traffic survey was done and the 60km/hour was chosen as design speed, Carriageway width of 7m and shoulder way of 1.5m was selected according to law N° 55/2011 of 14/12/2011. The obtained results indicated the thickness of sub base layer as 225mm, the thickness of road base as 170mm and surfacing layer as 100mm and the total road covered the length of 11.447 km.

Key Words: Traffic survey, geotechnical tests, geometric design, pavement design, Kabaya road

1. Introduction

The road is one of different infrastructures to respond to the requirements of the people's activities. Historically people have to travel and goods have been moved by different means of transportation, some of them is the road. As civilization developed and people's desire for communication increased, the design and techniques of construction vary time to time depending on economic, financial means, the materials available for construction and traffic loading by its growth rate over the design life. In practice, a road pavement structure is superimposed layers of selected and processed materials that is placed on well compacted soil or sub grade (Flaherty, 2002).

Once it is constructed, it will not last forever because with time, signs of destruction will appear referred to the number of traffics. These signs include cracking, cutting and polishing of the road's surface. A point will arrive where the road defects are at such an advanced stage that the integrity of pavement and hence the standard of service provided by it has diminished. Rehabilitation is required at this point to prolong the road's useful life. Loss of skid resistance and loss of texture are forms of deterioration that usually suffered by all Road pavements (Flaherty, 2002).

The combination of effects of traffic loading and the environment cause pavements to deteriorate over time. The deterioration effects need to be restored by adding or replacing material in the existing pavement or reconstruction of it. This term is known as rehabilitation which is a structural or functional enhancement of a pavement for producing a substantial extension in service life, by improving pavement condition and ride quality. Rwanda is a country in central Africa where economic activities and Tourism are progressively raising. Markets, health centers and Guest houses are numerous in its different towns and centers; one of them is Ngororero District. Since the country is getting more and more developed, the movement of Tourists, Population and their goods also increases, this requires sufficient transport means, particularly well-developed roads.

The road said in this case study connects the main road in Kabaya with very important infrastructures such as: Kabaya market, Kabaya police station, Kabaya hospital and Kabaya health center where a big movement of population is encountered. The structural state of this Road together with its geometrical elements has generated the thought of its geometrical and pavement design.

2. Problem Statement

The road section Kabaya faces problems of having sharp horizontal curves which are difficult for vehicles to negotiate, inappropriate visibility distances due to the buildings near the road and all these cause many accidents, its gradients were

steeper so that laden vehicles sometimes slide, its vertical profile was highly damaged so that stopping sight distances were not adequate, it had not shoulders, it had not cross fall and due to these, the potholes and gullies were developed from many years ago and cause different problems like damaging the springs of passing vehicles, waterlogging on the road's surface during winter seasons and weakness of underlying layers, it had not the side ditches for conveying the water coming from the catchment areas and on the pavement, due to this, the road's structure was damaged easily and activities of people near by the road of this case study always were damaged by the storm water due to lack of its management. In fact, all these problems make Kabaya road to be isolated and remain under developed compare to other centers in Kabaya district. By conducting road geometric design, pavement structural design and design longitudinal side ditches with appropriate standard and dimensions, the solutions about the problems counted between those centers would be obtained.

So the only solution was to provide new cross sectional elements which could support the mobility of the road users, horizontal elements with adequate radius of curvature and visibility sight distances, and vertical profile with the appropriate sight distances and allowable gradients to improve its capacity performance appropriate, to provide pavement structure which is capable of supporting the loads from traffics.

3. Materials and Methods

This section presents materials and methods used to achieve the targeted goal of the study. The research materials consisted of materials which are supposed to be used in topographic survey, construction of sub base courses, construction base courses of the road layers. All methods used within this research are presented in this section.

3.1 Description of study area

Kabaya road is located in western province of Rwanda, Ngororero district, Kabaya sector, specifically in Kabaya and Rurembo cells.

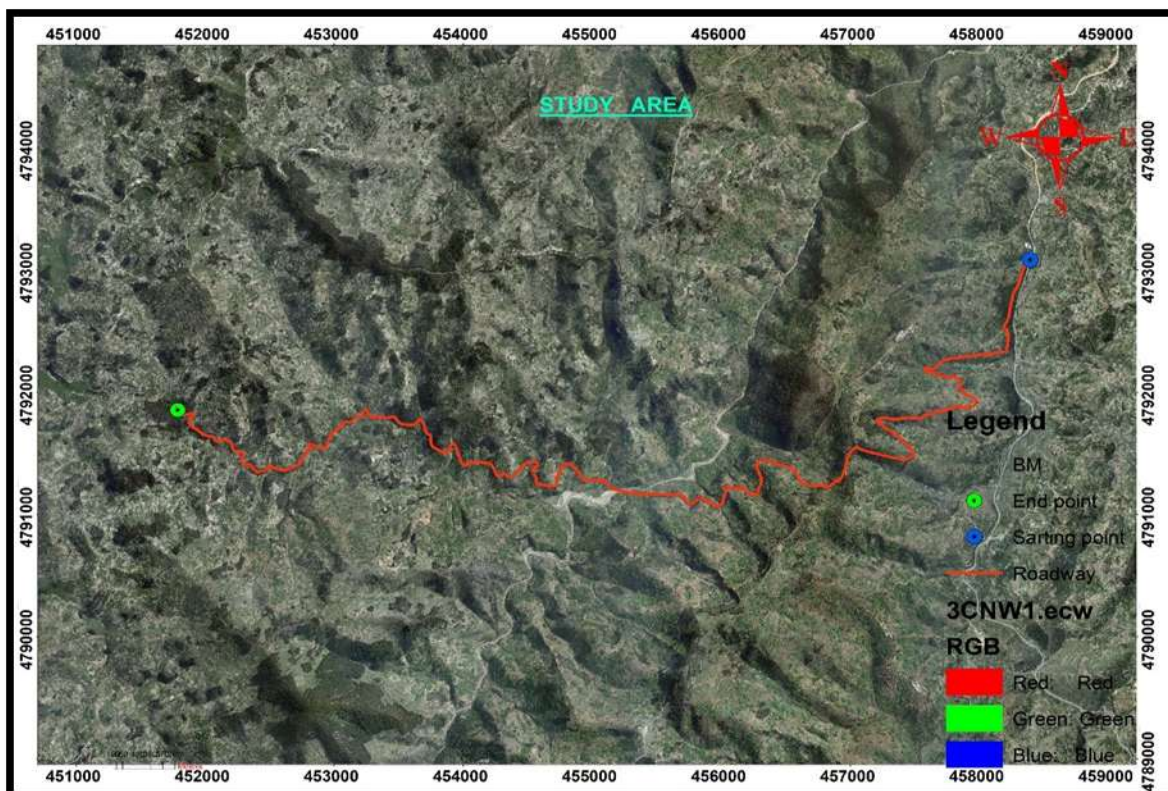


Figure-1: Kabaya road-Kabaya health centre

3.2 Terrain analyses and Selection of design standards

For this phase, consultation of Ngororero master plan was done for the purpose of analysing the site topography and then RTDA 2014 and AASHTO standard were chosen during the geometrical design.

3.3 Topographic survey

Topographic survey was carried out to gather more topographic coordinates and this leads determination of profile and cross-sectional drawings with full details to be used during implementation of this project. Field survey was carried out by three stages: reconnaissance survey, establishing of control point, topographic survey.

Reconnaissance survey

This was done as an exhaustive study which preliminarily done by analyzing aerial photos and then site survey of the land which was about to be surveyed. This was done both by arrival to the site and by aerial observation. The main purpose was to know exactly the different information available on the site and to choose suitable positions of the stations.

Establishing of control point

Table-1: Setting of control points

<i>STATION</i>	<i>X</i>	<i>Y</i>	<i>Z</i>
<i>B.M</i>	458381.666	4793113.137	1715.066
<i>R1</i>	458190.571	4792353.390	1725.946
<i>ST1</i>	457560.746	4792181.520	1761.743
<i>R2</i>	457987.476	4791914.487	1793.144
<i>ST2</i>	457186.769	4791773.442	1848.949
<i>R3</i>	457451.361	4791437.190	1860.432
<i>ST3</i>	457043.448	4791519.875	1884.194
<i>R4</i>	456767.970	4791219.401	1895.208
<i>ST4</i>	456310.411	4791445.424	1847.187
<i>R5</i>	456293.873	4791175.299	1832.617
<i>ST5</i>	456029.261	4791230.427	1810.871
<i>R6</i>	455969.017	4791055.791	1805.576
<i>ST6</i>	455832.882	4791139.566	1786.039
<i>R7</i>	454799.918	4791428.886	1785.073
<i>ST7</i>	454717.227	4791219.401	1785.139
<i>R8</i>	454540.819	4791346.195	1811.416
<i>ST8</i>	454557.357	4791450.937	1823.231
<i>R9</i>	454452.615	4791428.886	1832.216
<i>ST9</i>	454364.411	4791296.580	1824.973

3.4 Topographic Survey

Field survey was carried on the road Kabaya by use TS 06 total station, and by referring to the point of known elevation Bench Mark (B.M) to collect other coordinates.

3.5 Traffic survey and traffic forecasting

Traffic count was done by manual classified count method and it was done in 7 days, one count in weed-end and other three days in the week days.

Conversion of partially traffic counts into estimated full day counts

$$\text{Estimated full day count} = \frac{\text{Partial-day count}(06.00 \text{ to } 18.00) * (\text{Full 24-hour count})}{(\text{Count from 06.00 to 18.00 hours in the 24-hours survey})}$$

Calculation of design life Traffic

$$T_n = 365 * F_o \left(\frac{((1+r)^n) * p}{r} \right)$$

Calculation damaging Factor

$$D = \frac{0.35}{0.93^t + 0.082} - \left(\frac{0.26}{0.92^t + 0.082} \right) \left(\frac{1}{3.9^{(F+1550)}} \right)$$

Calculation of cumulative number of standard axle loads

Calculation of N , the cumulative number of standard axles $N = T_n * D$

3.6 Geometric design

Table-2: Stopping sight distance

S/N	INPUTS	Formula
Stopping site distance	V(km/h) =60, t(s)= 2.5, G (%) =7, g = 9.81, a = 3.4 m/sec ²	$D = vt + \frac{v^2}{2(a \pm Gg)}$

Table-3: Minimum length of rest curve

S/N	INPUTS	Formula
Minimum length of crest curve	S(m)=59.57, G1 (%) = 9.5, G2 (%) =7, h1=1.05, h2=0.2	$L = 2 * \left[S - \frac{100(\sqrt{h_1} + \sqrt{h_2})^2}{A} \right] \text{ For, } L \leq S$ $L = \frac{A * S^2}{200(\sqrt{h_1} + \sqrt{h_2})^2} \text{ For, } L \geq S$

Table-4: Minimum length of sag curve

S/N	INPUTS	Formula
Minimum length of sag curve	S(m)=59.57, G1 (%) = 9.5, G2 (%) =4.84, h1=1.05, h2=0.2	$L = 2S - \frac{200(\sqrt{h_1} + \text{Stan}\beta)}{A} \text{ For, } L \leq S$ $L = \frac{A * S^2}{200(\sqrt{h_1} + \text{Stan}\beta)} \text{ For, } L \geq S$

Table-5: Minimum length of sag curve under obstacle

S/N	INPUTS	Formula
Minimum length of rest curve under obstacle	S(m)=59.57), G1 (%) = 2.5, G2 (%) =4.66, h1=1.05, h2=0.2, CL=5.7	$L = \frac{[AS^2]}{800 \left[C - \frac{(h1 + h2)}{2} \right]} \text{ For, } L \geq S$ $L = 2S - \frac{800 \left[C - \frac{(h1 + h2)}{2} \right]}{A} \text{ For, } L \leq S$

Table-6: Horizontal alignment

S/N	INPUTS	Formulae
Minimum length Horizontal radius	v(km/h) =60, f = 0.15 eo=25, e=7	$R_{\min} = \frac{v^2}{127 \left(\frac{e}{100} + f \right)}$
Setback distance	S(m)= 59.57, R (m)=94.488	$M \geq R \left[1 - \cos \left(\frac{90+S}{\pi R} \right) \right]$
Minimum length Of transition curve	R(m)=94.488	$L_{\max} = \sqrt{24 * R}$
Shift	L(m)=47.620, R(m)=94.488	$S = \frac{L^2}{24 * R}$

3.7 Laboratory work

During the technical study of this research Comprehensive design of pavement of Kabaya road, Rwanda in the civil engineering laboratory test method, sample preparation, test procedures and reporting were referred to the laboratory soil testing books (Laboratory, 2000)

Sieve analysis: The sample into riffle box was subdivided using the cone-and-quarter method, 3kg of the sample were selected using scoop and mixed with water to form a slurry, the sample was washed through a sieve with an opening of 0.075mm until the water became clear while collecting some passing materials, the retained mass of the sample was put in the drying oven, after 24 hours the sample was removed from the drying oven and put immediately in the desiccators until it cooled, the dry mass was weighed to know the quantity of passed fine materials; then the dry sample was put in the mechanical sieve shaker and was shaken for 10min then for each sieve the mass retained weighed (Laboratory, 2000).

Proctor Test: This test is performed to reduce the liquefaction, permeability and compressibility under working loads (it is mostly done by reduce the voids and increasing the dry density) and this test was done with referring to standards of BS 1377 part 4, 1990. The main target of proctor test is done for obtaining the optimum moisture content and maximum dry density and those are the important values to be considered during soil compaction for making highway/road layers (Day, 2001).

CBR test : The CBR test was done based on the British standard as a reference (British Standards Institution, 1990). The California Bearing Ratio test noted as CBR test was used as measure of resistance of a material to penetration of standard plunger under controlled density and moisture conditions. It was developed by the California Division of Highways as a method

of classifying and evaluating soil subgrade and base course materials for flexible pavements (Day 2001; Oregon Department of transportation 2019).

Liquid limits: Consistency is term used to indicate the degree of firmness of cohesive soils. The physical properties of clay greatly differ at different water contents and this test was done by referring (Department transportation, 2019). A soil which is very soft at a higher percentage of water content becomes very hard with decrease in water content (British Standards Institution, 1990).

4. Results and interpretations

Referred to the results obtained in the below Table7; it is found that the terrain on which the road is supposed to pass is mountainous.

Table-7: Terrain analysis

Max Elevation(m)	Min Elevation(m)	Average gradient (%)	Terrain classification (Number of contours)
2216	2125	6	30

According to Robinson & Thagesen, (2004) terrain is mountainous.

4.1 Traffic forecasting

Conversion of partially traffic counts into estimated full day counts

The average daily traffic

$$408 + 486 + 398 + 816/4 = 526 \text{ Veh/day}$$

Where heavy vehicles correspond to 30 % (155veh/day) and light vehicles correspond to 70% (371 veh/day).

Table-8: Traffic forecasting

Damaging factor	Design life Traffic (msa)	Cumulative Number of Standard Axles (msa)
D=4.136	tn =1.870	7.73~ 8

The ORN 29 and 31 methods are valid for designs up to 40 and 30 million standard axles respectively (Rogers, 2003). So, it means that this project can be conducted by referring to these standards.

4.2 Design geometric parameters

Table-9: Calculated horizontal alignment elements

Horizontal alignment						
V(Km/h)	emax %	Fmax	Radius R(m)	Transition curve length(m)	Shift(m)	Visibility distance(m)
60	7	0.15	94.488	47.62	1	6.58

Table-10: Vertical alignment

Vertical alignment			
K	Crest curve length (m)	sag curve length (m)	
63.8	19.14	---	
39.41		35.47	

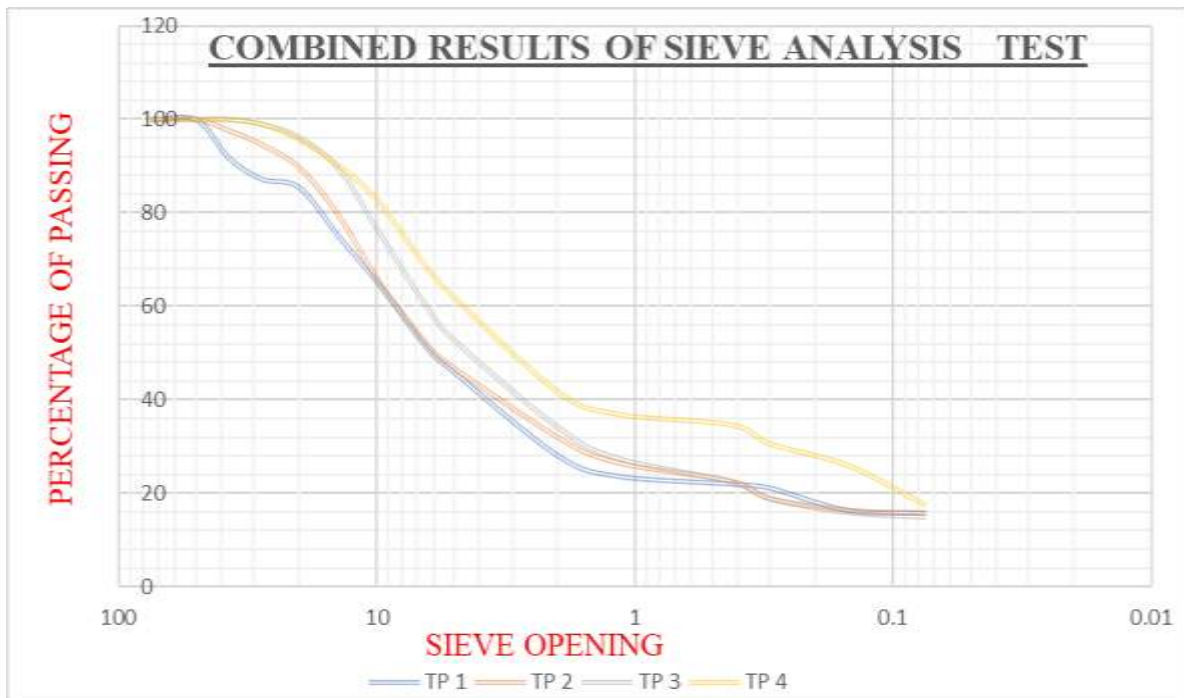
Table-11: Calculated stopping sight distance elements

Stopping sight distance			
V(km/h)	t (sec)	a (m/sec ²)	Distance D (m)
60	2.5	3.4	59.57

4.3 Tests for subgrade soil

Table-12: Results of sieve analysis test

SIEVE ANALYSIS								
Sieve size(mm)	sample I		sample II		sample III		sample IV	
	% Retained	% Passing	% Retained	% Passing	% Retained	% Passing	% Retained	% Passing
75	0	100	0	100	0	100	0	100
50	0	100	0	100	0	100	0	100
37.5	8.1	91.9	2.4	97.6	0	100	0	100
28	12.7	87.3	5.4	94.6	1	99	1	99
20	14.5	85.5	10.3	89.7	3.8	96.2	4.3	95.7
14	25.1	74.9	20.7	79.3	10.7	89.3	10	90
10	34.7	65.3	34.1	65.9	23.5	76.5	17.2	82.8
6.3	49.3	50.7	48.6	51.4	40.8	59.2	32.2	67.8
5	54.2	45.8	53.3	46.7	47.4	52.6	38.2	61.8
2	71.9	28.1	68	32	65.9	34.1	58.2	41.8
1.18	76.3	23.7	73.4	26.6	72.6	27.5	63	37
0.425	78	22	77.4	22.6	77.6	22.4	65.3	34.7
0.3	78.9	21.1	81.1	18.9	81.3	18.7	69.4	30.6
0.15	83.7	16.3	83.6	16.4	84.2	15.8	74	26
0.075	84.2	15.8	84.3	15.7	85.2	14.8	82.6	17.4



Chat-1: Combined results of sieve analysis

Table-13: Soil classification based on AASHTO

Classification					
Collected sample	% passing (NO 10)	% passing (NO 40)	% passing (NO 200)	soil group	Soil class
sample I	28.1	22	15.8	A-1-b	Gravels
sample II	32	22.6	15.7	A-1-b	Gravels
sample III	34.1	22.4	14.8	A-1-a	Gravels
sample IV	41.8	34.7	17.4	A-1-b	Gravels

Granular materials (F200<35%)

Table-14: Soil classification by ASSHTO

Group classification		A-1		A-3
		A-1-a	A-1-b	
Sieve analysis (percentage)	No. 10	50 max		
	No. 40	30 max	50 max	51 min
	No. 200	15 max	25 max	10 max
Characteristic of fraction passing No. 40	Liquid Limit		
	Plasticity index	6 max		NP
Usual types of materials		Stone fragments, gravel and sand		Fine sand

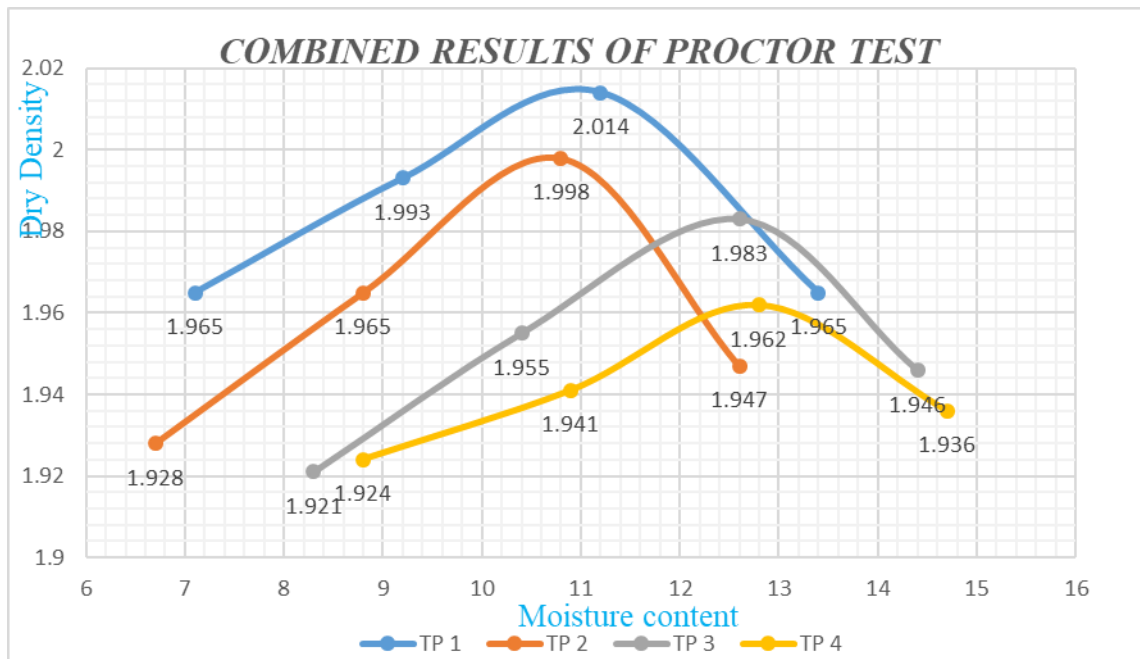
$$GI = (F - 35)[0.2 + 0.005(LL - 40)] + 0.01(F - 15)(PI - 10)$$

$$GI = (15.8 - 35)[0.2 + 0.005(26.3 - 40)] + 0.01(15.8 - 15)(8.6 - 10) = 0$$

Based on the obtained results from the above table, the tested construction material (soil) samples were classified as **stone fragments, gravel and sand** material with no presence of clay and it was classified as **gravel material** with respect to (AASHTO) and ASTM (D3282-09). The percentage of granular material is in the range of 82.6-85.2 (% retained on sieve No 10 + % retained on sieve No 40 + % retained on sieve No 200) with group index of zero which is the best construction material for subgrade since it is inversely proportional to Group Index.

Table-15: Results for Proctor test

COMBINED RESULTS OF PROCTOR TEST							
Sample I							Classification
DD	1.965	1.993	2.014	1.965	MDD	2.014	Quite good
MC %	7.1	9.2	11.2	13.4	OMC	11.2	good
Sample II							
DD	1.928	1.965	1.998	1.947	MDD	1.998	good
MC %	6.7	8.8	10.8	12.6	OMC	10.8	good
Sample III							
DD	1.921	1.955	1.983	1.946	MDD	1.983	good
MC %	8.3	10.4	12.6	14.4	OMC	12.6	good
Sample IV							
DD	1.924	1.941	1.962	1.936	MDD	1.962	good
MC %	8.8	10.9	12.8	14.7	OMC	12.8	good



Chat-2: combined results of proctor test

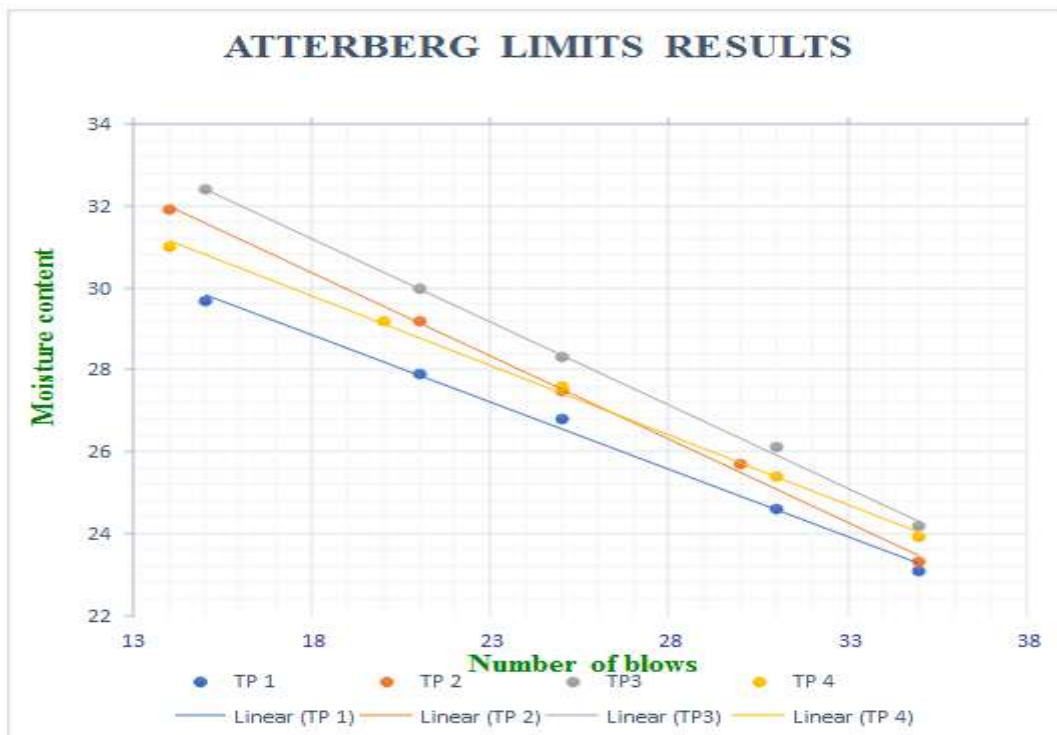
After conducting compaction test and based on the obtained results of optimum moisture contents (OMC) and maximum dry densities (MDD) as shown in the above Figure 3, the results showed that the collected samples I, was classified as quit good

materials since its Maximum dry density is in the range of 1.3 to 2.4 while II,III and IV were classified as good materials as it is in the range of 1.6 to 2.0 by referring to AASHTO(1978) designation T180 and ASTM (1980) designation D 1557.

Table-16: Results of Atterberg limits test

ATTERBERG LIMITS TEST								
LIQUID LIMITS					PLASTIC LIMIT		PLASTIC INDICES	
<i>Sample I</i>								
Blows	15	21	25	31	35	WL	Plastic limit	Plastic Indice
MC (%)	29.7	27.9	26.8	24.6	23.1	26.3	18.2	8.6
<i>Sample II</i>								
Blows	14	21	25	30	35	WL	Plastic limit	Plastic Indice
MC (%)	31.9	29.2	27.5	25.7	23.3	27.3	17.7	9.8
<i>Sample III</i>								
Blows	15	21	25	31	35	WL	Plastic limit	Plastic Indice
MC (%)	32.4	30	28.3	26.1	24.2	28.3	17.9	10.4
<i>Sample IV</i>								
Blows	14	20	25	31	35	WL	Plastic limit	Plastic Indice
MC (%)	31	29.2	27.6	25.4	23.9	27.7	18.5	9.2

According to Garber & Hoel (2002), Since this soil is found in A-1-a and A-1-b, thus the soil is granular material and can be used as a subgrade or sub base material satisfactorily if properly drained, in addition, such soils must be well compacted and protected with an adequate thickness of pavement for the surface load to be supported. The following figure presents Atterberg limits results from the above table 15 for sample1, Sample 2, Sample 3 and Sample 4.

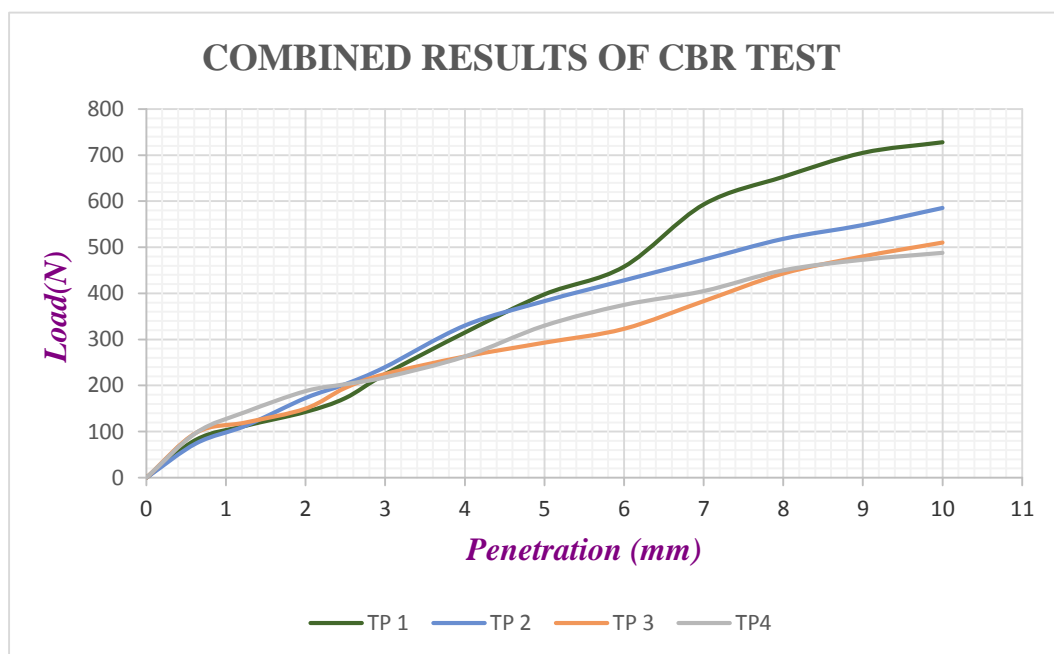


Chat-4: Combined results of Atterberg limits test

Table-17: Results of CBR test

Sample I													
Penetration(mm)	0	0.63	1.25	2	2.5	3	4	5	6	7	8	9	10
Load (KN)	0	83	113	143	173	225	315	398	458	593	653	705	728
Sample II													
Penetration(mm)	0	0.63	1.25	2	2.5	3	4	5	6	7	8	9	10
Load (KN)	0	75	113	173	203	240	330	383	428	473	518	548	585
Sample III													
Penetration(mm)	0	0.63	1.25	2	2.5	3	4	5	6	7	8	9	10
Load (KN)	0	98	120	150	195	225	263	293	323	383	443	480	510
Sample IV													
Penetration(mm)	0	0.63	1.25	2	2.5	3	4	5	6	7	8	9	10
Load (KN)	0	98	143	188	203	218	263	330	375	405	450	473	488

CBR Calculation					
	blows	Penetration(mm)	Load(N)	Formula	Results (%)
Sample I	55	5	398	(19.35/1.05)	19
Sample II	55	5	383	(19.35/1.05)	18
Sample III	55	5	293	(19.35/1.05)	15
Sample IV	55	5	330	(19.35/1.05)	16
Design CBR	Result (%)				
Average CBR x 2/3	11.33				



Chat-4: combined results of CBR test

After conducting CRB test, the obtained results from Table 16 and Figure 4 indicated that design CBR is 11.5 % and according to Rogers (2003), in the below table 17, this CBR value is satisfactory for subgrade construction material.

Pavement structural design

The below Table 17 indicates the thickness requirements for both sub base material alone and combination of sub base and capping for different CBR values of the underlying subgrade materials (Rogers, 2003)

Table-17: The required thickness based on CBR value

Layer	CBR of subgrade				
	<2	2	3	4	5
Sub base thickness(mm)	615	400	310	260	225
Sub base + Capping comprising					
-Sub base thickness(mm)	150	150	150	150	225
-Capping layer thickness (mm)	600	350	350	350	---

According to Rogers (2003), the sub base and capping layer act as a regulator of the surface of the sub-grade below and protect it against the effects of inclement weather. They are along with the subgrade, provide a secure platform on which the upper layers of the highway pavement can be built. The dominant of the thickness of this pavement section is the strength of the underlying subgrade. Its design is independent of cumulative traffic incident on the upper layers of the pavement over its design life. For subgrade in excess of 5% CBR, the required sub base depth is no greater than 225mm, down to a minimum of 150mm at a subgrade CBR of 15 % (HD 25/94).

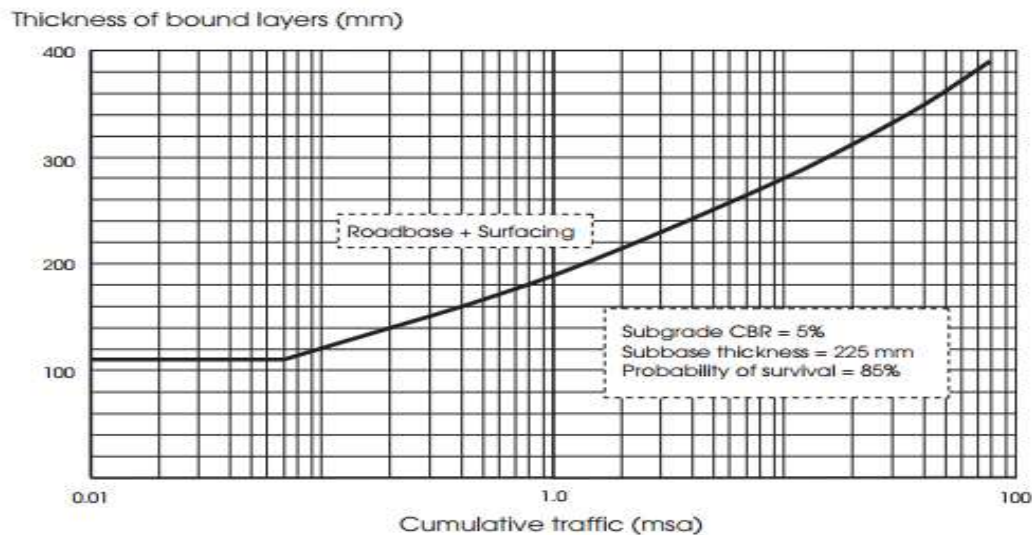


Figure 2: Showing Design curve for highways with bituminous road base. Source: (Rogers, 2003)

Granular and cement based sub base are recommended for flexible pavements (HD25/94).

In the case of unbound sub bases, their high stiffness modulus, relatively impermeable to water though not of necessity free draining. Their laboratory CBR should be a minimum of 30 %. According to the above theories the thickness of structural pavement of this case study should be 170mm since its design CBR is 11.33 %. And from these equivalent standard axle loads together with design curve for highways with bituminous road base found as a figure (2-15) in chapter two, the base course+surfacing layer was found to be 160mm (155mm for road base and 5mm for surfacing) (Rogers, 2003).

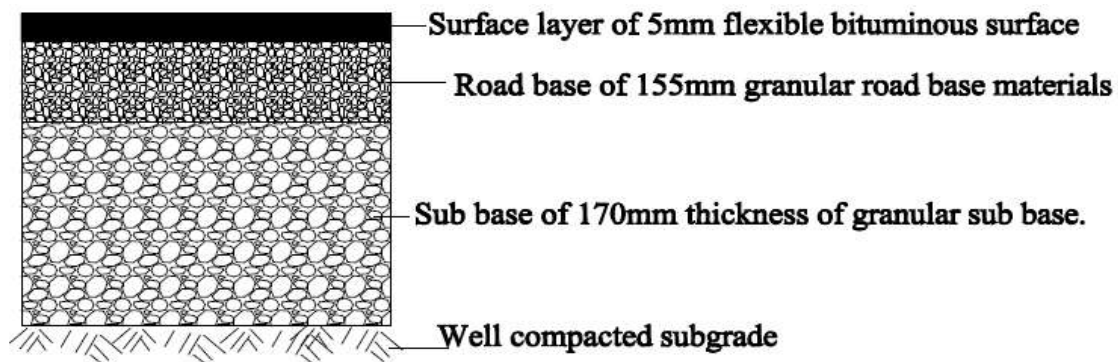


Figure 3: Typical section of pavement structure

5. Concluding Remarks

Kabaya road was designed to meet the projected traffic and Ngororero master plan layout requirements as it was the main objective of the study. The geometric design has been achieved by following AASHTO design procedure. In fact, geometrical parameters such as stopping sight distance, vertical curve length, simple horizontal curve radius and transition curve has been calculated using a prepared spread sheet to complete road geometric design input parameters. The design covered 11.447 km, where the 60 km/hour was chosen as design speed and a carriageway width of 7m and width of the shoulder 1.5m.

In addition, this project involved the selection of appropriate pavement and surfacing materials to ensure that the pavement of the road section said in the case study will perform adequately the functions for which it is designed and will require minimal maintenance under the anticipated traffic loading for the design period adopted. It has given the appropriate thickness and composing materials for that road section to withstand traffic loads passing on it. The project provided a road section of width that is minimized so as to reduce the cost of construction and the maintenance, whilst being sufficient to carry the traffic loading efficiently and safely. The pavement surface is covered by an impermeable layer for the protection of the foundation which can be softened by the entrance of water if it is not adequately treated.

The results found are as follow: minimum horizontal radius was found to be 95m corresponding transition curve was found to be 47.74m, stopping site distance was found to be 59.57m, crest curve length was found to be 19.14m, sag curve length was found to be 35.47m, according to the results obtained from sieve analysis the soil was found to be gravel soil, design CBR was found to be 11.33%.

6. Acknowledgements

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