

Development of Special Tool with Fixture for Process Optimization of Hex Key Hole

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Abstract — The Competitive atmosphere in manufacturing sector is primarily driven by customer demand for products that are durable and cost effective without a compromise on quality. These requirements trickle down to all the processes such as design, validation, prototyping and production that are involved in delivering a product to customers meeting their requirements. While the quality aspect is usually achievable by using modern production methods such as Electrical Discharge Machining, the cost effectiveness aspect gets diminished. Therefore, a balance must be achieved so that the criteria for both quality and cost effectiveness can be met. This paper postulates one such balanced methodology for development of special tool with a fixture for hex key hole cutting.

The specialized tool is designed using Solid works CAD software package based on the critical design variables such as the dimensions of key hole, depth of keyhole, etc. The tool is then analyzed using classical analytical techniques. These results are in turn validated with finite element analysis using Altair HYPERWORKS Software package.

The material selected for specialized tool with fixture is HSS and is developed for utilization on lathe. The benefits of this methodology is decrease in cost of machining by 20 times and reduction in production time by 10 times all the while maintaining same level of quality in the output.

Keywords—Broaching, Hex key, Lathe, EDM, FE Analysis.

I. INTRODUCTION

The competitive atmosphere in manufacturing sector has made it mandatory that unorthodox methodologies are developed that are a perfect mix of disruptive innovations and classical machining processes and equipment. This in turn ensures that the newly developed methodologies are easy to adopt both in terms of process setup and manpower training. The focus of this paper is a specialized tool developed for use on lathe such that this combination can compete with processes like Electrical Discharge Machining (EDM) [1] in terms of process time, production costs and output quality.

The operating principle of the tool is that of a rotary broaching. Rotary broaching is a very useful way of producing hexagonal or other polygonal holes in metal. It can also be used to produce internal splines and other profiles. It is especially useful for producing such profiles in short blind holes.

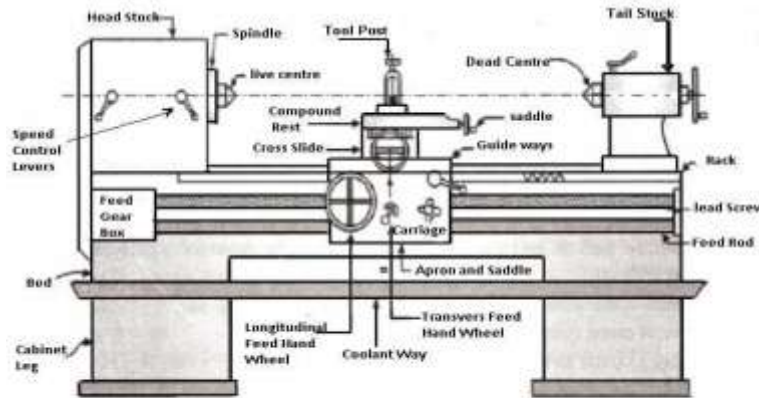
The principle of rotary broaching is quite straight forward [2]. A hole is drilled in the work piece with a diameter of slightly more than the minimum cross section diameter of the shape to be broached. With the work piece rotating under power a shaped cutter that can freely rotate is brought up to the hole at a slight angle and it is pressed into the hole. The rotating work piece causes the cutter to revolve and, because of the slight angle, the corners of the cutter come into contact in turn, each taking a peck as it does so. After one revolution the cutter has shaved a little metal from the hole, and as the tool is fed into the hole during subsequent revolutions, the hole is gradually broached to the shape of the cutter until the required depth is reached.

The material selected for the tool is traditional HSS due to its availability and versatility. The fidelity of tool is inspected using analytical methods which are then validated with simulation results.

II. LITERATURE REVIEW

[Meenu Sahu] [Komesh Sahu] They developed an optimization method of the cutting parameters (cutting speed, depth of cut and feed) in dry turning of AISI D2 steel to achieve minimum tool wear, low work piece surface temperature and maximum material removal rate (MRR) [3]. The experimental layout was designed based on the Taguchi's L9 (3⁴) Orthogonal array technique and analysis of variance (ANOVA) was performed to identify the effect of the cutting parameters on the response variables. The results showed that depth of cut and cutting speed are the most important parameter influencing the tool wear. The minimum tool wear was found at cutting speed of 150 m/min, depth of cut of 0.5

In the process of hex key hole cutting, the job is held in the four jaw chuck or three jaws chuck depending on the accuracy required for the job and tool is fed from the tailstock with using the special designed revolving type holder. This creates a shearing effect around the edges of the form being cut. Essentially only a section of the form is being cut at any given time – which greatly reduces the amount of cutting pressure needed to form the desired feature.



LATHE MACHINE

Fig. 3. Representational Image of Lathe Machine

The tool holder has a spindle which spins independently of the rest of the holder. Thus, when we are producing the internal hex key hole on a lathe, when the tool meets the rotating part, it begins spinning at the same rate as the part /Job rotating and feed is given by the rotating the tail stock. In this process the tool shape is transferred on to the job and depth is controlled with feeding of tailstock.

Figure 4 shows the specialized tool with fixture that is used for hex key hole cutting. Figure 5 shows the special tool being used for hex key hole cutting.



Fig. 4. Special Tool with Fixture



Fig. 5. Hex Key Cutting Operation

IV. DESIGN CALCULATION FOR SPECIAL TOOL

Analytically cutting forces and thrust forces are calculated by using different depth of cut (d) and feed rate (f) are as follows:

For d = 0.5 mm and f = 0.5 mm/rev

$$F_c = 1593 \times f^{0.85} \times d^{0.98} \text{ N}$$

$$= 1593 \times 0.5^{0.85} \times 0.5^{0.98}$$

$$F_c = 448.05 \text{ N}$$

Where d = Depth of Cut f = Feed rate

Fc = Cutting Force Thrust Force Calculation

Average co-efficient of friction on the tool face, $\mu = 0.7$

Rake angle, $\alpha = 3^\circ$

$$\mu = \frac{F_c \tan \alpha + F_t}{F_c - F_t \tan \alpha}$$

$$0.7 = \frac{448 \tan 3 + F_t}{448 - F_t \tan 3}$$

Thrust Force, $F_t = 279.85 \text{ N}$

Similarly, other calculations are done by using above formulae for different depth of cut and feed rate are tabulated in Table 1 as follows:

Feed Rate (mm/rev)	Depth of Cut (mm)	Cutting Force Fc (N)	Thrust Force Ft (N)
0.5	0.5	448.05	279.85
	1	883.77	552.12
	1.5	1314	820.82

Table 1. Calculation of Forces During Operation

Similarly, the stress on tool can also be calculated. For

Depth of Cut = 0.5 mm

$$\frac{r \cos \alpha}{1 - r \sin \alpha}$$

Shear angle $\tan \phi = \frac{r \cos \alpha}{1 - r \sin \alpha}$ $\tan \phi = \frac{0.1235 \cos 3^\circ}{1 - 0.1235 \sin 3^\circ}$

$$\phi = 7.074^\circ$$

Normal Force $F_n = F_c \sin \phi + F_t \cos \phi$

$$F_n = 448 \sin 7.074^\circ + 279.85 \cos 7.074^\circ$$

$F_n = 332.892 \text{ N}$

$$\sigma = \frac{F_n}{A_s}$$

= 163.87 MPa

Similarly, stress induced can be calculated for depth of cut of 1 mm and 1.5 mm. This is tabulated in Table 2.

V. STRUCTURAL ANALYSIS OF SPECIAL TOOL

The CAD geometry of the tool is modelled using solid modelling software package SOLIDWORKS. The CAD data is then converted to Initial Graphics Exchange Specification (IGES/STP) format and imported into pre-processing software Altair HYPERMESH. The tool is discretized by meshing process into 3d tetra elements [6]. A sensitivity check is performed to ascertain the correct mesh size suitable for the analysis. The element size ultimately selected is a range of 0.8mm to 4mm. Additionally, fine mesh is provided in the stress concentration zones such like tool tip and taper end neck. The tool is then analyzed using OPTISTRUCT solver [7]. The post- processing of results is then done in HYPERWORKS.

The Stress are plotted with respect to different depth of cut i.e. for 0.5 mm, 1 mm and 1.5 mm.

Figure 6. shows the stress plot for depth of cut of 0.5 mm. The maximum stress of 184 MPa is noted at the interacting tip of the tool. It is to be noted that another critical area, the taper neck, has to be evaluated. The Maximum stress in this zone is 177 MPa. Both the values are well below the Yield limit of HSS.

Therefore, tool will not fail in these conditions.

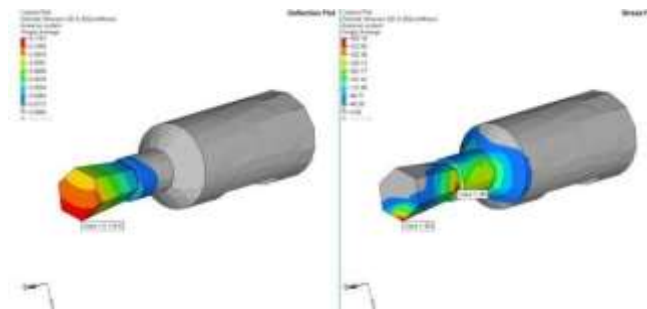


Figure 6. Deflection and stress plot for 0.5mm Depth of Cut

The results for depth of cut of 1.0 mm is shown in Figure 7. The stress at the interacting tool tip is 363 MPa and in the taper neck area is 349 MPa. It is again well below the Yield limit of HSS. Therefore, tool will not fail in these conditions.

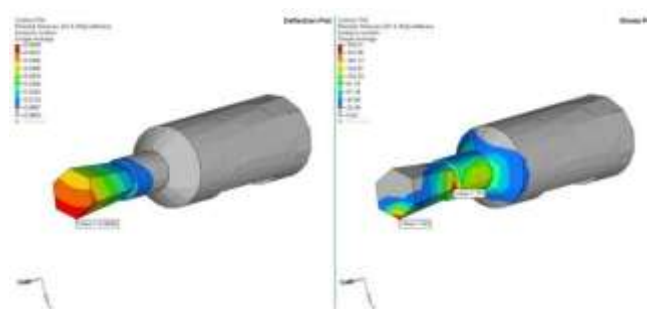


Figure 7. Deflection and stress plot for 1 mm Depth of Cut

The results for depth of cut of 1.0 mm is shown in Figure 8. The stress at the interacting tool tip is 363 MPa and in the taper neck area is 349 MPa. It is again well below the Yield limit of HSS. Therefore, tool will not fail in these conditions.

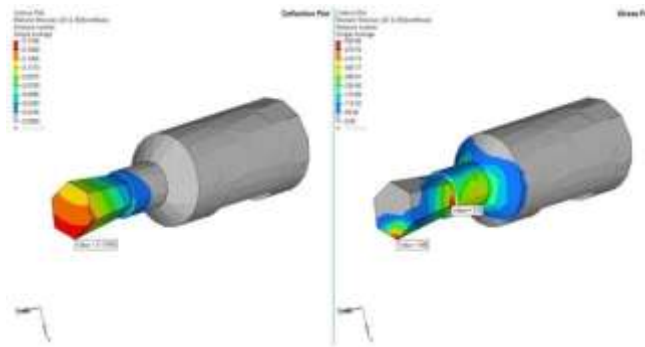


Figure 8. Deflection and stress plot for 1.5mm Depth of Cut

VI. CONCLUSION AND FUTURE SCOPE

There is good correlation between the two sets of results as seen in Table 2. It is clear that with increase in depth of cut stress on cutting tool also increases. When both F_c and F_t applied on cutting tool is stress maximum. Stress is nearly equal when both F_c and F_t and only F_c are applied. But stress on cutting tool due to thrust force is less as compared to cutting force.

Depth of cut	Analytically Calculated Stress (MPa)	Stress by FEM Analysis (MPa)	Correlation
0.5	163.87	184.01	89%
1	301.14	363.83	83%
1.5	507.7	539.66	94%

Table 2. Correlation of Analytical and FE Analysis Results

It can also be seen that there is good correlation between analytical results and FEA based results thereby validating the design of the tool.

The benefits of this methodology is decrease in cost of machining by 20 times and reduction in production time by 10 times all the while maintaining same level of quality in the output.

For future scope, this methodology can be applied and studied further for various other metallic and non-metallic materials for tool making. There is also scope for expanding this study to include effects of temperature on fidelity of the special tool.

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