

“STATIC STRUCTURAL AND MODAL ANALYSIS OF SECONDARY AIR FLOW SYSTEM”

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Abstract - Secondary air flow system play a significant role in turbine engine to accomplish reliable operation of the individual modules as well as the whole engine. Main functions of secondary air flow system are to provide cooling flow to engine components, to seal bearing chamber and to control bearing axial loads. Being a functional discipline, secondary air flow system owns the air flow that is essentially not the primary flowpath. In this study, solid modelling of Secondary air flow system having trapezoidal cross-section referring to one of its existing design is done using CATIA V5. Further, analyses are carried out in ANSYS Workbench. Further, Modal analysis is carried out to determine the vibration characteristics such as natural frequencies and mode shapes. The combination of frequency and amplitude is found to be efficient method for reducing or controlling forces which generate stress.

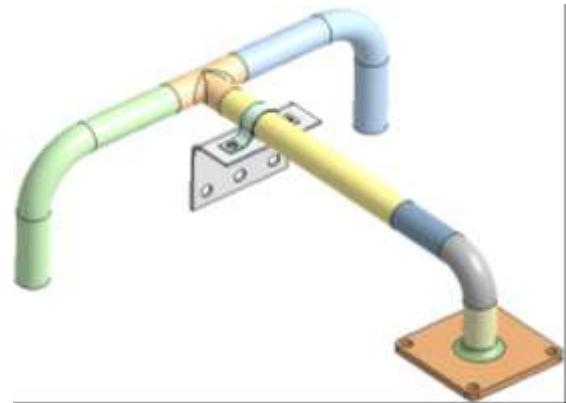


Fig 1.0 Secondary air flow system

Keywords— Secondary air flow system, Static Analysis, Modal Analysis, Ansys 18.1

1. INTRODUCTION

An aircraft engine is the component of the propulsion system for an aircraft that generates mechanical power. Internal heat gain due to electrical and mechanical equipment used in engine and the blade will try to grow radially and there is possibility to expand and touch the casing of aero plane engine which causes catastrophic failure. To avoid this failure, we need to cool the engine blade by providing less hot air from the compressor. To provide this less hot air one tubing structure will be present inside the engine which is known as “Secondary Air Flow System”. This system is connected to engine casing (very stiff) by L- bracket and flange. This structure is situated between 4th stage of High Pressure Compressor (HPC) and the engine blade side casing.

1.1 Literature Survey

Following literatures are studied,

Airflow control system for supersonic inlets”. Mitchell, G.A.

In this paper they have done an invention to provide a new and controllable air bleed system for the inlet of supersonic air craft engine. Yet another object of the invention is to provide a controllable air bleed system which responsive to a substantially constant bleed pressure characteristics control device. An additional object of the invention is to provide a controllable air bleed system for supersonic inlets where in massive amount of air may be bypassed from the throat of a supersonic inlet.

“Heat Transfer inside Compressor Rotors: Overview of Theoretical Models”

J. Michael Owen, Hui Tang and Gary D. Lock

Increasing pressures in gas-turbine compressors, particularly in aero engines where the Pressure ratios can be above 50:1, require smaller compressor blades and an increasing focus on Blade clearance control. The blade clearance depends on the radial growth of the compressor discs, which in turn depends on the temperature and stress in the discs. As the flow inside the disc cavities is buoyancy-driven, calculation of the disc temperature is a conjugate problem: the heat transfer from the disc is coupled with the air temperature inside the cavity. The flow inside the cavity is three-dimensional, unsteady and unstable, so computational fluid dynamics is not only expensive and time-consuming, it is also unable to achieve accurate solutions at the high Grash of numbers found in modern compressors. Many designers rely on empirical equations based on inappropriate physical models, and recently the authors have produced a series of papers on physically-based theoretical modeling of buoyancy-induced heat transfer in the rotating

cavities found inside compressor rotors. Predictions from these models, all of which are for laminar flow, have been validated using measurements made in open and closed compressor rigs for a range of flow parameters representative of those found inside compressor rotors.

2. Material Properties

Materials selected for Secondary air flow system are inconel-625 and inconel-718 Alloy the properties of materials are given below in Table 2.1

Property/Material	Inconel-625	Inconel-718
Young's Modulus (Mpa)	2.08E+05	2.00E+05
Poisson's Ratio	0.278	0.294
Yield Strength(Mpa)	1034	517
Ultimate Strength (Mpa)	1241	965

Table 2.1 Material properties

3. Modeling of secondary air flow system

The Secondary air flow system is modeled using CATIA V5 as shown in below fig.

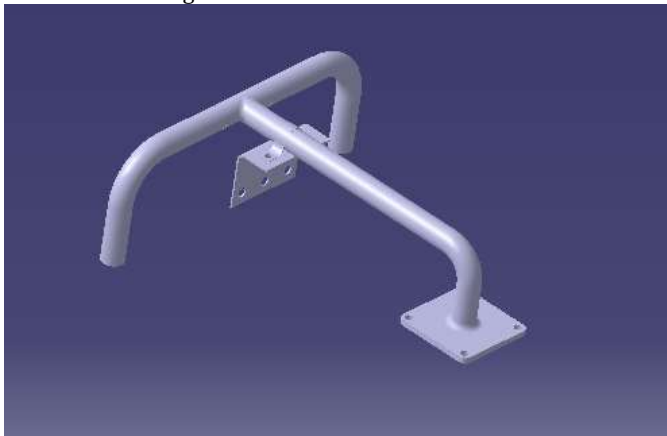


Fig. 3.1 3-D solid model

4. Finite Element Analysis using Ansys

The finite element analysis (FEA) is a numerical technique for solving problems which are described by partial differential equations or can be formulated as functional minimization.

Meshing

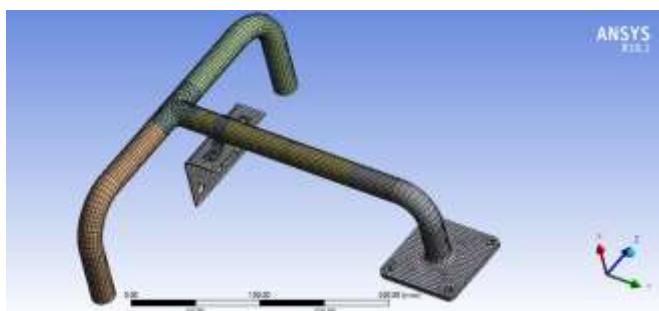


Fig 4.1 Meshed Model

Boundary Conditions

Fixed Support 1

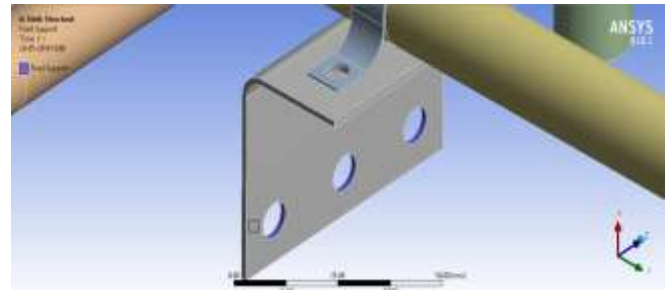


Fig 4.2 Fixed Support 1

Fixed Support 2

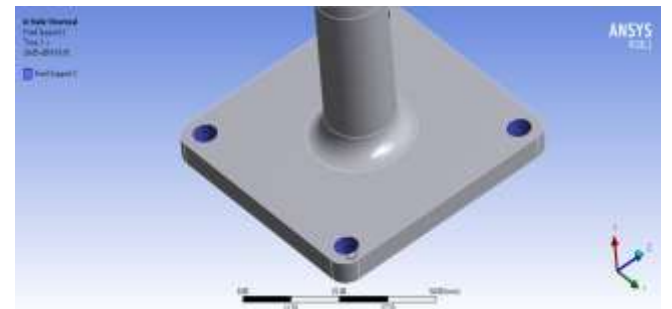


Fig 4.3 Fixed Support 2

Loading Condition

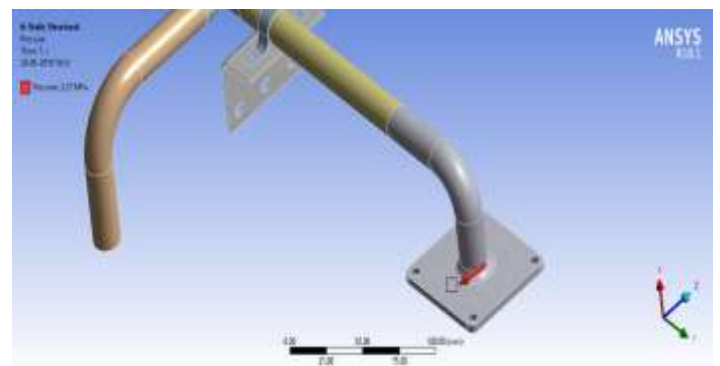
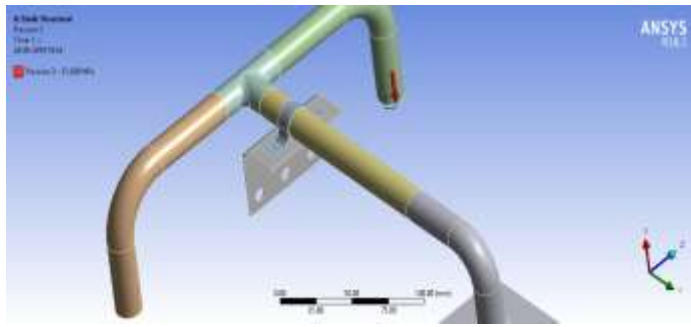


Fig 4.4 Applied pressure 1



Section		
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• Pipe	• Stress (Mpa)	
	• FEA	• Analytical
• Straight Pipe Section	27.2	27.6
• Bend Pipe Section	32.1	33.1
• Bend Pipe Section	64.5	66.1

Table 5.3 Burst pressure

• Pipe	• Stress (Mpa)	
	• FEA	• Analytical
• Straight Pipe Section	36.3	36.4
• Bend Pipe Section	42.4	43.7

Fig 4.5 applied pressure 2

5. Analytical Calculations

$$\sigma = Pd/2t$$

Where,

σ = Stress in N/mm²

P = Pressure in Mpa

d = internal diameter of pipe in mm

t = Thickness of pipe in mm

5.1 Normal Pressure

$$\sigma = Pd/2t = (2.27 * 17.6) / (2 * 0.725) = 27.6 \text{ Mpa}$$

Table 5.1 Normal pressure

5.2 Proof Pressure

$$\sigma = Pd/2t = (2.99 * 17.6) / (2 * 0.725) = 36.4 \text{ Mpa}$$

Table 5.2 Proof pressure

5.3 Burst Pressure

$$\sigma = Pd/2t = (4.54 * 17.6) / (2 * 0.725) = 55.1 \text{ Mpa}$$

• Pipe	• Stress (Mpa)	
	• FEA	• Analytical
• Straight Pipe	55.2	55.1

6. RESULTS AND DISCUSSION

Equivalent Stress

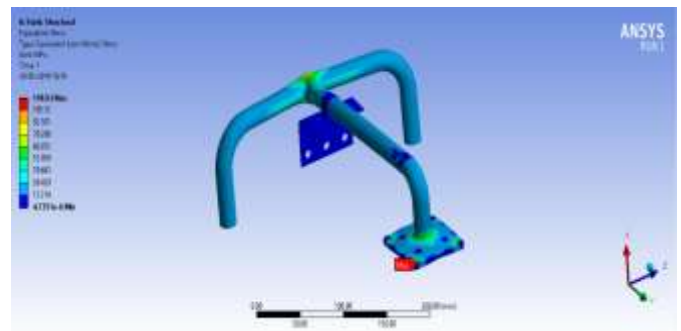


Fig 6.1 Equivalent Stress 1

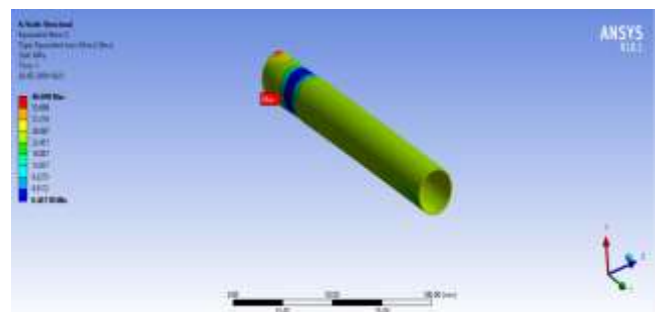


Fig 6.2 Equivalent Stress 2

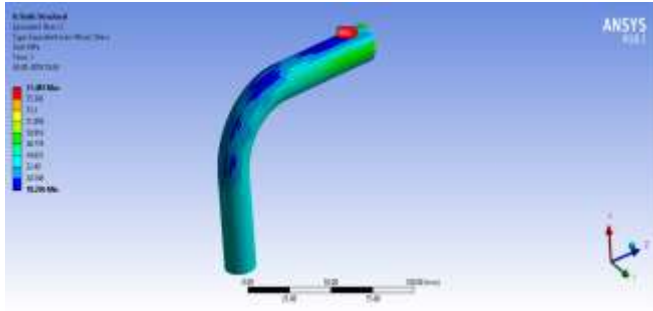


Fig 6.3 Equivalent Stress 3

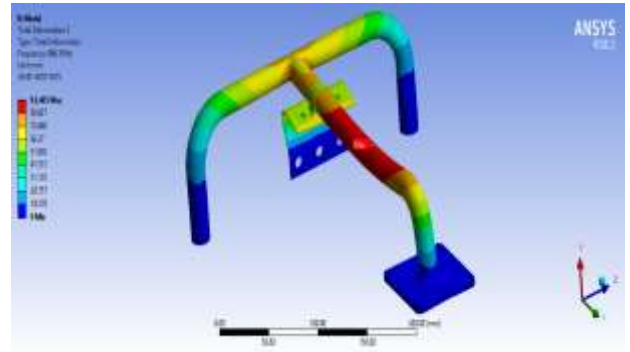


Fig 6.7 Total Deformation 2 B

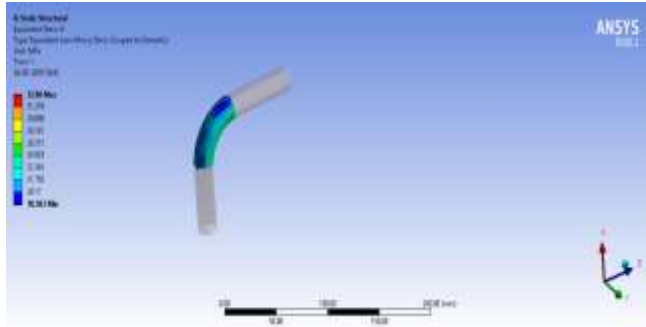


Fig 6.4 Equivalent Stress 4

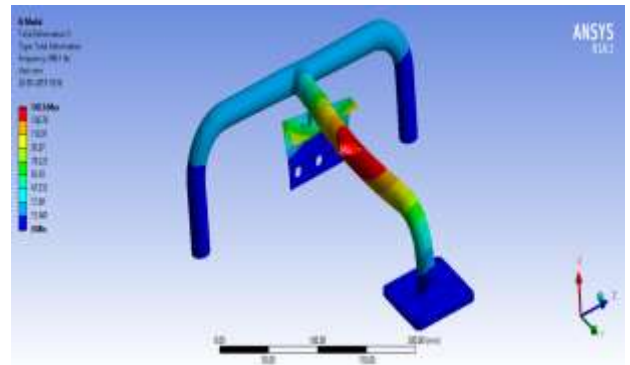


Fig 6.8 Total Deformation 3 B

Total Deformation

- STATIC STRUCTURAL

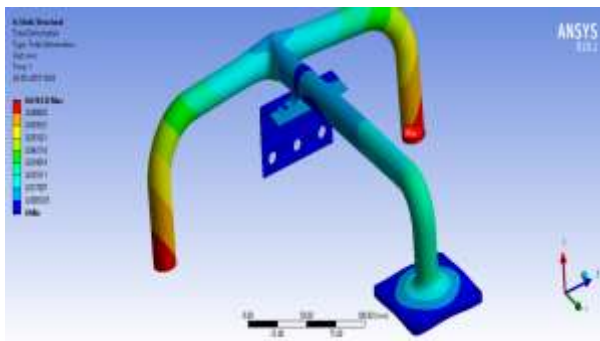


Fig 6.5 Total Deformation A (SS)

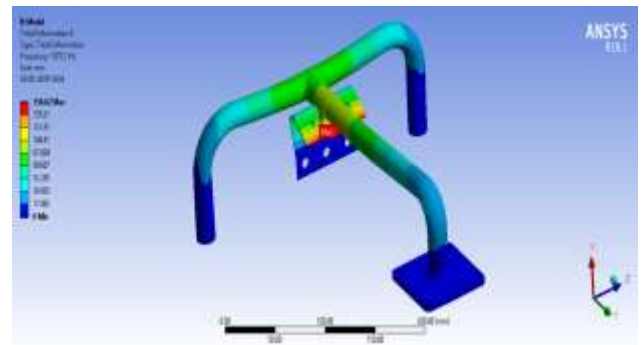


Fig 6.9 Total Deformation 4 B

- Modal

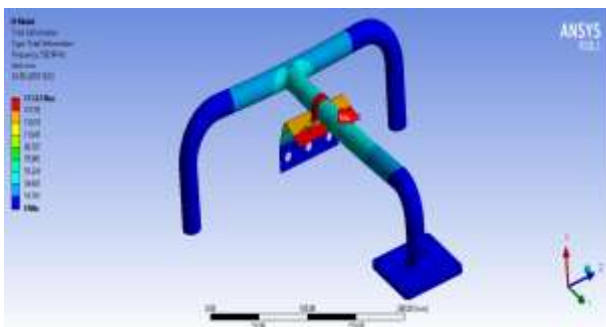


Fig 6.6 Total Deformation 1 B

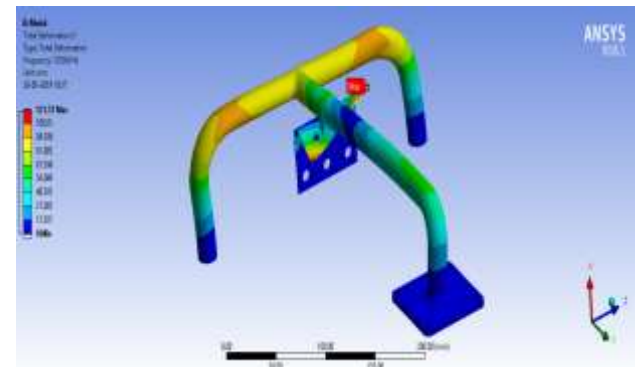


Fig 6.9 Total Deformation 5 B

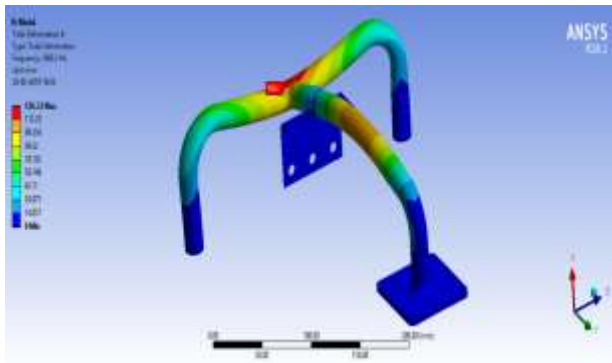


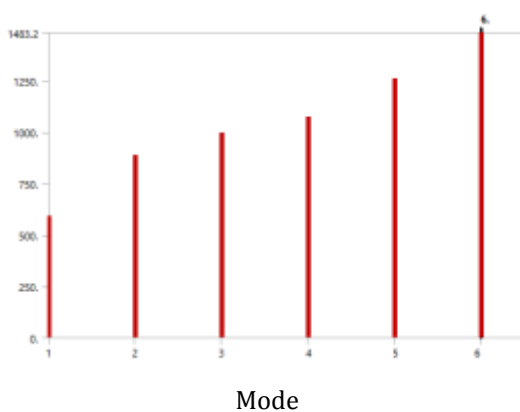
Fig 6.10 Total Deformation 6 B

Frequency (Hz)

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6. **"Heat Transfer inside Compressor Rotors: Overview of Theoretical Models"** J. Michael Owen, Hui Tang and Gary D. Lock

Frequency at each calculated mode.



Graph 6.1 Frequency at each calculated mode.





Mode	Frequency [Hz]
1.	592.94
2.	886.18
3.	998.1
4.	1073.3
5.	1259.6
6.	1483.2

Table 6.1 Frequency vs Mode

7. Conclusion

- Air flow system is meeting the design requirements for normal, proof and burst fluid pressure
- Air flow system is having factor of safety more than in all loading conditions
- Analytical results are closely matching with FEA results
- Critical frequencies and resonance condition will be checked from modal analysis.
- First fundamental frequency is observed at 576.6Hz and it is away from excitation frequency

BIOGRAPHIES

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