

COMPARATIVE STUDY ON SCC WITH PARTICLE PACKING DENSITY AND EFNARC DESIGN

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Abstract:- Self-compacting concrete (SCC) is an innovative concrete that does not require vibration for placing and compaction. The hardened concrete is dense, homogeneous and has the same engineering properties and durability as traditional vibrated concrete. The self-compacting concrete flows easily at suitable speed into formwork without blocking through the reinforcement without being heavily vibrated. This project deals with the self-compacting concrete where the cement is partially replaced with fly-ash. Here Ordinary Portland Cement is replaced with 20% of fly-ash. The mix design particle packing density is used to determine the proportion of concrete ingredient and comparing with the EFNARC 2005 guideline. This work summarizes the experiments for evaluating the performance of self-compacting concrete including V-funnel, L-box, J-ring and slump flow tests as well as the recent achievements of the fresh and hardened properties of self-compacting concrete such as slump flow, segregation resistance is studied for the different water cement ratio and compressive strength and tensile strength for corresponding mix determined.

Keywords: Self Compacting Concrete, flow ability, passing ability, resistance to segregation, fly ash, Super plasticizer.

1. INTRODUCTION

Self-compacting concrete (SCC) is an innovative concrete that does not require vibration for placing and compaction. The hardened concrete is dense, homogeneous and has the same engineering properties and durability as traditional vibrated concrete.

Self-compacting concrete (SCC) was first developed in Japan in the late 1980's as a concrete that can flow through congested reinforcing bars with elimination of compaction, and without undergoing any significant segregation and bleeding. In recent times, this concrete has gained wide use in many countries for different applications and structural configurations. Adoption of SCC offers substantial benefits in enhancing construction productivity, reducing overall cost, and improving work environment. Therefore, the first point to be considered when designing SCC is to restrict the volume of the coarse aggregate. This reduction necessitates the use of higher volume of cement which increases the cost, besides resulting in undesirable temperature rise. So, cement should be replaced by other mineral admixtures like Blast Furnace Slag, Fly Ash, Silica Fumes, etc. The usage of mineral admixtures in the production of SCC not only provides economic benefits but also reduces heat of hydration. A very limited work is reported from India, non-mechanization of the construction industry, abundant

availability of construction materials available at very low cost. There for it can be said that SCC is still quite unknown to many researchers, builders, ready mix concrete production, academia etc. There are non-coda references for the mix design of high-grade Concrete. Mix designs for high grade concrete can be done by particle packing density Method. This is a new concept of mix design.

The packing density is the ratio of volume of solids to the total bulk volume. The Particle Packing gives indirect measurement of geometry of the concrete mix and also gives the cement paste to be required to fill the Void content in the concrete. To achieve the optimized particle packing density, particle is selected in such a way that small size particles fill up the Voids between the larger particles and so on. The Voids between the aggregate particles are filled by the cement paste and the excess of the paste will be a solid coating around each aggregate present in the mix. For the optimized packing density of aggregate small amount of paste content is required to fill the Voids.

2. MATERIALS USED

2.1 Cement

The OPC 43 grade which is used in the study conforming to IS12269:1987.

2.2 Coarse Aggregate

Coarse aggregate crushed granite of size 10 mm used as coarse aggregate. The sieve analysis of coarse aggregates confirms to the specifications of IS 383:1970 for graded aggregate and specific gravity 2.72, Water Absorption 1.70%, and Impact value 12.67%.

2.3 Fine Aggregate

M-sand is used as a fine aggregate conforming to the requirements of IS: 383 - 1970. The M-Sand is artificially manufactured sand, consisting of particles of different sizes proportioned to suite the requirement of Fine Aggregates to be used in structural concrete. The M - Sand used in the mix has a specific gravity of 2.37, Water absorption of 8.5%, Loose Bulk Density of 1580kg/m³ and Roded Bulk Density of 1860kg/m³.

2.4 Water

The potable water available in the laboratory, satisfying the requirement of IS 456-2000 is used for mixing the HPC and also curing all the concrete specimens, PH of water used is almost neutral (7).

2.5 Mineral Admixture

Fly Ash Fly ash is a fine inorganic material with pozzolanic properties, which can be added to SCC to improve its properties.

2.6 Chemical Admixture

Master Glenium Sky 8233 is an admixture of a new generation based on modified polycarboxylic ether. The product has been primarily developed for applications in high performance concrete where the highest durability and performance is required. It is used to increase the workability and reduce water content in the concrete.

Physical and chemical properties of Master GleniumSky 8233

Table 2.1 Physical and chemical properties

Form	Liquid
Colour	Brown
Odour	characteristics
Boiling point	>100°c
p ^H	6-9

3. MIX DESIGN PROCEDURES

3.1 EFNARC Mix design

EFNARC The mix sequence is determined as:

1. Designation of desired air content (mostly 2 %)
2. Determination of coarse aggregate volume
3. Determination of sand content
4. Design of paste composition
5. Determination of optimum water: powder ratio and super plasticizer dosage in mortar
6. Finally, the concrete properties are assessed by standard tests.

3.2 Particle Packing Density Mix Design

The mix design is carried Out Using Particle packing density approach method. The loose and roded bulk density of M - Sand and Coarse aggregates are evaluated separately. The following steps are adopted to calculate the design mix for further Work to Curry out.

1. Determination of packing density.
2. Estimation of voids Content and voids ratio.
3. Calculation of packing factor.
4. Evaluate the mass of the fine aggregate and coarse aggregate.
5. Determining the mass of total aggregates.
6. Finding out the required cement paste and by selected the W / C.
7. Estimation of cement content and also quantity of water required.

4. RESULTS AND DISCUSSION

4.1 Slump Flow Test

The slump assessment carried out by varying the dosage of admixture is noted for each trial. The trial is stopped when the wet mix exhibits the required workability in term of slump flow.

Table 4.1 Slump Flow Test Result as per EFNARC and PPD design

W/C ratio	Admixture dosage in (%)	EFNARC Slump Spread Horizontal in (mm)	PPD Slump Spread Horizontal in (mm)
0.30	2	650	680

0.33	1.8	630	650
0.35	1.6	600	620
Value		600-800	

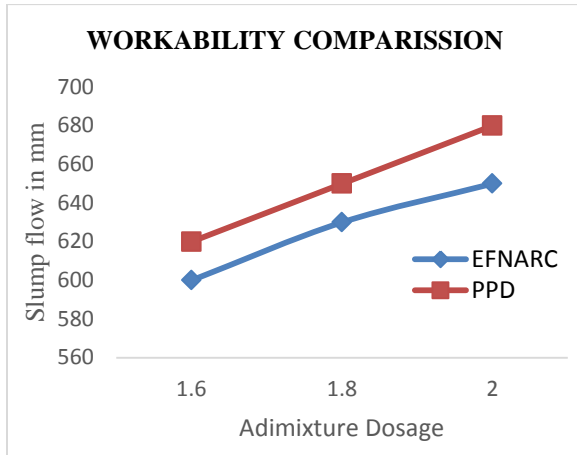


Fig 1 Typical variation graph for Slump flow variation Adimixture Dosage

4.2 Funnel Test

Conformation results of V funnel test for both mixes is tabulated below

Table 4.2 Result of V Funnel Test as per EFNARC design

W/C ratio	Admixture dosage in (%)	V Funnel	
		Tr flow (sec)	Flow at T5(sec)
0.30	2	12	15
0.33	1.8	11	14
0.35	1.6	9	12
Value		≤ Tr+3	

Table 4.3 Result of V Funnel Test as per PPD design

W/C ratio	Admixture dosage in (%)	V Funnel	
		Tr flow (sec)	Flow at T5(sec)
0.30	2	14	17
0.33	1.8	13	16
0.35	1.6	11	14
Value		≤ Tr+3	

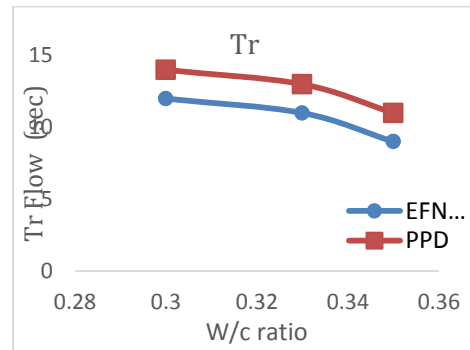


Fig 2 Typical variation graph for V Funnel flow Tr with water cement ratio

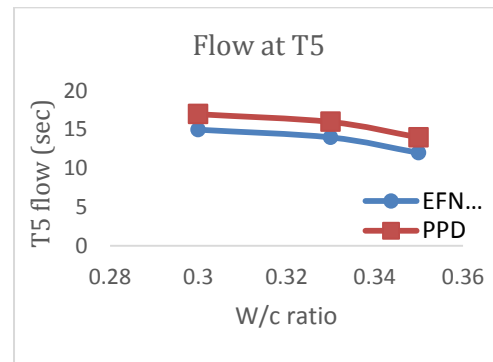


Fig 3 Typical variation graph for V Funnel flow T5 with water cement ratio

4.3 L Box Test

Conformation results of L box for the both mix is tabulated below

Table 4.4 Result of L Box Test as per EFNARC and Particle Packing Density design

W/C ratio	Admixture dosage in (%)	EFNARC Blocking ratio (H2/H1)	PPD Blocking ratio (H2/H1)
0.30	2	0.8	0.85
0.33	1.8	0.85	0.9
0.35	1.6	0.95	1
Value		0.80-1.0	

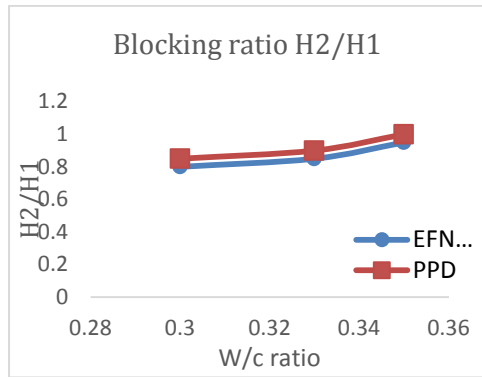


Fig 4 Typical graph for L Box Blocking ratio at different water cement ratio

4.5 J Ring Test

Conformation results of J ring test for both the mixes tabulated below

Table 4.5 Result of J Ring Test as per PPD design

W/C ratio	Admixturer dosage in (%)	EFNARC Difference in height (h1-h2) in mm	PPD Difference in height (h1-h2) in mm
0.30	2	8	8
0.33	1.8	6	7
0.35	1.6	4	5
Value		0-10	

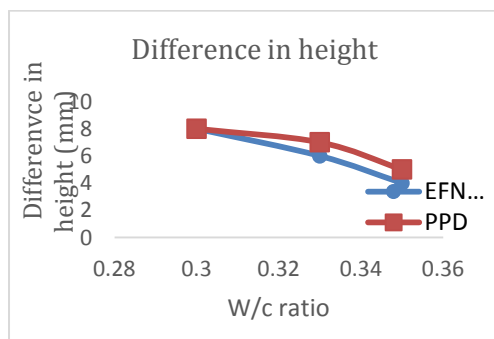


Fig 5 Typical graph for J ring difference in height water cement ratio.

4.6 Compressive strength

A compressive strength of these both concrete mix cubes are evaluated and strength is assessed after 7 days and 28 days of curing. The size of the test specimen is 150x150x150mm cubes results are tabulated below.

A. Compressive strength as per EFNARC design

Table 4.6 Compressive Strength of SSC

SL No	No of days Testing	Compressive strength in N/mm ²	Average compressive strength, N/mm ²
01	07	30.66	31.19
02		31.82	
03		31.11	
01	28	41.77	42.41
02		42.88	
03		42.75	

B. Compressive strength as per Particle Packing Density design

Table 4.7 Compressive Strength of SSC

SL No	No of days Testing	Compressive strength in N/mm ²	Average compressive strength, N/mm ²
01	07	39.37	39.11
02		38.84	
03		39.11	
01	28	49.80	49.80
02		49.20	
03		50.20	

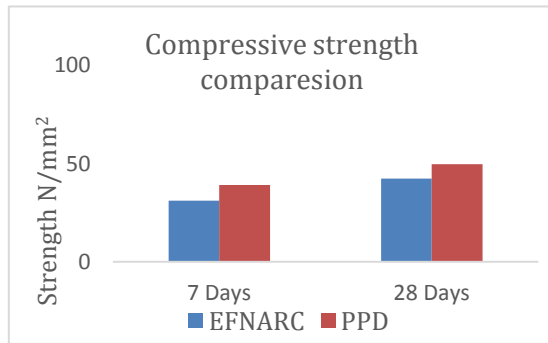


Fig 6 Graph of Compressive Strength Comparison

01	28	3.50	3.56
02		3.48	
03		3.68	

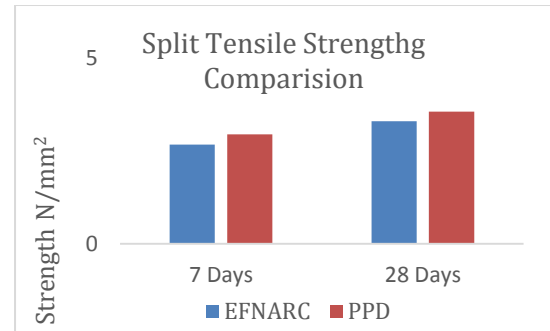


Fig 7 Graph of Split Tensile Strength Comparison

4.7 Split tensile strength

A split tensile strength of these both concrete mix beams is evaluated and strength is assessed after 7 day and 28 days of curing. The size of the test specimen is 150mm diameter and 300mm height.

A. Split tensile strength as per EFNARC design

Table 4.8 Tensile Strength of SSC

SL No	No of days Testing	Tensile strength in N/mm²	Average Tensile strength, N/mm²
01	07	2.532	2.677
02		2.716	
03		2.773	
01	28	3.11	3.30
02		3.46	
03		3.24	

B. Split tensile strength as per particle packing density design

Table 4.9 Tensile Strength of SSC

SL No	No of days Testing	Tensile strength in N/mm²	Average Tensile strength, N/mm²
01	07	2.80	2.95
02		2.97	
03		3.08	

CONCLUSIONS

Compressive Strength: It has been observed that the compressive strength of SCC as per the EFNARC design and particle packing density at the end of 28 days is 42.41 N/mm² and 49.80 N/mm² respectively. Comparing the both mix design the higher strength is achieved by particle packing density method.

Split Tensile Strength: It has been observed that the split tensile strength of SCC as per the EFNARC design and particle packing density at the end of 28 days is 3.30 N/mm² and 3.56 N/mm² respectively. Comparing the both mix design the higher strength is achieved by particle packing density method.

From the investigation on rheology of SCC mixes, it may be concluded that the admixture dosage at which the flow properties could be achieved in general is nearly 1.6% to 2%, If the W/C ratio decreases the high dosage admixture is required to achieve workability. the result of particle packing density mix design is compared with the EFNARC 2005 specification guideline.

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