

Planning, Analysis and Designing of Cantilever Residential Building

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Abstract - The project is about planning, analysis and designing of cantilever residential building. It is a framed structure, the residential building is located near to ooty. The total area of building is 100.3 sq.m. The plan and reinforcement details drawn by using Auto-CADD. Analysis done by Manual Calculation. Design are worked by referring code books.

Key Words: Ground Floor size :100.35 sq.m, First Floor area :100.35 sq.m, No of Floors :G+1

1. INTRODUCTION

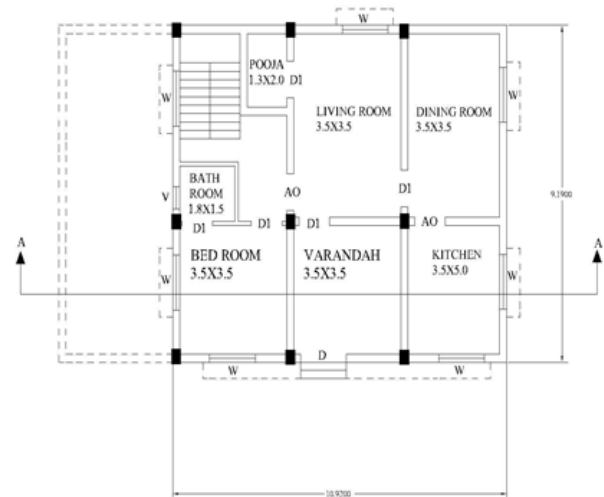
The basics needs of human existences are food, clothing and shelter. From times immemorial man has been making efforts in improving their standard of living. The point of his efforts has been to provide an economic and efficient shelter. Every human has an inherent like on a peaceful environment for his pleasant living this objective is achieved by having a place for living, situated at a safe and convenient location. Such a place for comfortable and pleasant living is required to all. Construction is the important aspects of civil engineering. Mankind has been evolving different kinds of environment with the change in civilization and time.

2. METHODOLOGY

- Plan of the Building
- Design of Cantilever Slab
- Design of Cantilever Beam
- Design of Column
- Design of Footing
- Design of Staircase
- Conclusion

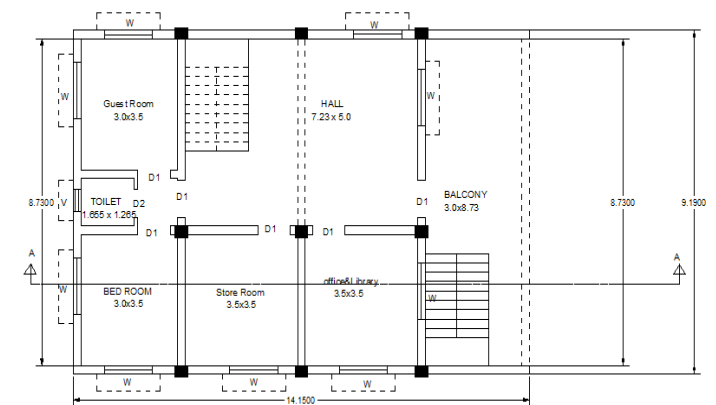
2.1 Plan of the building

Ground Floor Plan



ALL DIMENSION ARE IN m

First Floor Plan



ALL DIMENTIONS ARE IN m

2.2 Design of Cantilever Slab

Span = 3 m
 Live Load = 3 KN/m²
 Floor Finish = 1 KN/m²
 M20 & Fe 415 grade

Calculation of Depth of Slab:

$$d = \text{Span}/7$$

$$= 3000/7$$

$$d = 428.57 \text{ mm} = 460 \text{ mm}$$

Over all Depth = Depth of Slab + Cover

Assume Cover = 20 mm

$$D = 480 \text{ mm}$$

Load Calculation:

$$\text{Self Weight of Slab} = 0.2 \times 25 = 5 \text{ KN/m}$$

$$\text{Floor Finish} = 1 \text{ KN/m}$$

$$\text{Live Load} = 3 \text{ KN/m}$$

$$\text{Total Load} = 9 \text{ KN/m}$$

$$\text{Ultimate Load} = 13.5 \text{ KN/m}$$

Maximum Bending Moment,

$$M_u = W_u l^2 / 2$$

$$= 70.42 \text{ KN.m}$$

Maximum Shear Force,

$$V_u = W_u l = 43.60 \text{ KN}$$

Calculation of Limiting Moment of Resistance:

$$M_{u \text{ limit}} = 0.138 f_{ck} b d^2$$

$$= 584.01 \text{ KNm}$$

$$M_u < M_{u \text{ limit}}$$

Hence it is Under Reinforced Section

Calculation of Area of Steel:

$$M_u = 0.87 f_y A_{st} d (1 - f_y A_{st} / f_{ck} b d) \quad (1-)$$
$$70.42 \times 10^6 = 0.87 \times 415 \times A_{st} \times 460$$
$$415 A_{st} / 20 \times 1000 \times 460$$
$$A_{st} = 432.43 \text{ mm}^2$$

To Find Main Ast Provided:

$$\text{No of bars} = A_{st} / a_{st}$$

$$\text{Assume dia} = 10 \text{ mm So } a_{st} = 78.53 \text{ mm}^2$$

$$\text{So No of bars} = 6 \text{ Nos}$$

$$A_{st \text{ Provided}} = 6 \times \pi / 4 \times 10^2$$

$$= 471.23 \text{ mm}^2$$

$$A_{st \text{ Req}} < A_{st \text{ Pro}}$$

Hence Safe

Calculate Spacing of Steel:

$$\text{Spacing} = 1000 A_{st \text{ Of 1 bar}} / \text{Area of Steel}$$

$$\text{Area of 1 bar} = \pi / 4 \times d^2$$

$$\text{Assume dia} = 10 \text{ mm} = 78.53 \text{ mm}^2$$

$$\text{Spacing} = 190 \text{ mm}$$

Check for Spacing:

$$1) 300 \text{ mm}$$

$$2) 3d = 3 \times 460 = 1380 \text{ mm}$$

$$3) 190 \text{ mm}$$

Hence Provide 8 mm dia bars @ 190 mm c/c

Check Distribution Area of Steel:

$$= 0.12 \% \text{ of gross area}$$

$$= 552 \text{ mm}^2$$

To Find Distribution Ast Provided:

$$\text{No of bars} = A_{st} / a_{st}$$

$$\text{Assume dia} = 8 \text{ mm So } a_{st} = 50.26 \text{ mm}^2$$

$$\text{So No of bars} = 12 \text{ Nos}$$

$$A_{st \text{ Provided}} = 12 \times \pi / 4 \times 8^2$$

$$= 603.16 \text{ mm}^2$$

$$A_{st \text{ Req}} < A_{st \text{ Pro}}$$

Hence Safe

Calculate Spacing of Steel:

$$\text{Spacing} = \text{Area of one bar} / \text{Area of steel}$$

$$= 90 \text{ mm}$$

Check for Deflection:

$$(L/d)_{\text{max}} > (L/d)_{\text{pro}}$$

$$(L/d)_{\text{max}} = B.V \times K_t \times K_c$$

$$= 9.59$$

$$(L/d)_{\text{pro}} = \text{Span} / \text{Eff depth}$$

$$= 7.02$$

$$9.59 > 7.02$$

Hence Safe

2.3 Design of Cantilever Beam

To Find Over all Depth:

$$\text{Length of cantilever} = 3 \text{ m}$$

$$M.F = 1$$

$$\text{eff depth} = \text{span} / 7 \times M.F$$

$$= 3000 / 7 \times 1$$

$$= 428 \sim 430 \text{ mm}$$

$$\text{effective cover} = 25 \text{ mm}$$

$$\text{Overall depth of beam} = 430 + 25$$

$$= 455 \text{ mm}$$

To Find Effective Depth:

$$\text{Provide an overall depth of } 460 \text{ mm}$$

$$\text{Effective depth } d = 460 - 25$$

$$= 435 \text{ mm}$$

To Find Dead Load Moment: = 6.35

Let the section of cantilever be,
 230 mm x 435 mm at fixed end
 $2/3 \times d = 2/3 \times 435$
 = 290 mm
 230 mm x 290 mm at free end
 D.L of the cantilever = $(0.435 + 0.29/2) \times 0.23 \times 3 \times 25000$
 = 6253.13
 Load acts at a distance = $\{(0.435 + 2 \times 0.29) / (0.435 + 0.29)\} \times 3/3$
 = 1.4 m from fixed end
 D.L moment = 6253.13×1.4
 = 8754.4 Nm

**To Find Live Load Moment:
 From Wall:**

Live load = $3 \times 0.23 \times 2$
 = 13.8 KN/m
 Total live load = $13.8 + 15.93$
 = 29.73 KN/m
 Live load moment = $wl^2/2$
 = $29.73 \times 3^2/2 = 133.78$ KNm

To Find End Load Moment:

End point load = $2.5 + 1.75$
 = $4.25 \times 0.35 \times 25 = 37.18$ KN/m
 End load moment = W.L
 = $37.18 \times 3 = 111.56$ KN/m
 Total moment = E.M + L.L.M + D.L.M
 = $111.56 + 133.78 + 8.75$
 = 254.09 KNm

To Find Limiting Moment:

Total load = $(29.73 + 8.75) \times 3 + 37.18$
 = 152.62 KN
 $M_u = 254.09 \times 1.5$
 = 381.135 KNm
 $M_u \text{ limit} = 2.76 \text{ bd}^2$
 = $2.76 \times 230 \times 460^2 = 134.32$ KNm

To Find Area of Tension & Compression Reinforcement:

Percentage of steel required,
 $P_t = 25/460$
 = 0.05
 $M_u / \text{bd}^2 = 381.135 / (0.23 \times 0.46^2)$

Tension zone:

$A_{st} = 2.002/100 \times 230 \times 460^2$
 = 974.3 mm²
 $A_{sc} = 1.091/100 \times 230 \times 460^2$
 = 530.91 mm²

To Find No of Bars:

No of bars use 20 dia bars,
 Use 4 Nos of 20 dia @ tension zone
 No of bars at compression zone
 Use 16 mm dia
 No of bars = $530.91 / (\pi/4 \times 16^2)$
 = 2.67 ~ 3 Nos

To Find Check for Shear:

$\tau_v = V_u / \text{bd}$
 $V_u = (152.62 \times 103) / (230 \times 460)$
 = 1.53 N/mm²
 $\tau_c = 100 A_{st} / \text{bd}$
 = $(100 \times 974.3) / (230 \times 460)$
 = 0.597 N/mm²
 $K \tau_c = 1 \times 0.59$
 = 0.59 N/mm²
 $\tau_{c \text{ max}} = 2.8$ N/mm²
 $\tau_v < K \tau_c < \tau_{c \text{ max}}$
 Hence Safe

2.4 Design of Column

To Find Axial Load:

$B = 300$ mm
 $D = 400$ mm
 $L = 3.5$ m
 $M_{u1} = Wl^2/12 = 27.68 \times 3.5^2/12 = 37.44$ KNm
 $M_{u2} = Wl^2/12 = 18.68 \times 3^2/12 = 14.01$ KNm
 $M_u = M_{u1} + M_{u2} = 51.45$ KNm
 $51.45 = Wl^2/8 = W_u \times 6.5^2/8$
 $W_u = 9.74$ KN/m
 $P_u = 9.74 \times 6.5 = 63.32$ KN

To Find Non-Dimensional Parameters:

$d' = 40$ mm
 $D = 400$ mm
 = 0.1
 From chart – 32,
 $M_u / f_{ck} b D^2 = 51.45 \times 10^6 / (20 \times 300 \times 400^2) = 0.05$

$$P_u/fck b D = 63.32 \times 10^3 / (20 \times 300 \times 400) = 0.026$$
$$P/fck = 0.2, P = 4$$

To Find Reinforcement:

$$A_s = p_b D / 100 = 4 \times 300 \times 400 / 100 = 4800 \text{ mm}^2$$

Adopt 25 mm dia

$$n = 4800 / (\pi / 4 \times 25^2) = 8 \text{ Nos}$$

To Provide Lateral Ties:**Condition:****Diameter:**

$$5) \frac{1}{4} \times 25 = 6.25 = 6 \text{ mm}$$
$$6) \text{ Less than } 16 \text{ mm}$$

Spacing:

$$7) \text{ LLD} = 300 \text{ mm}$$
$$8) 16 \times 25 = 400 \text{ mm}$$
$$9) 300 \text{ mm}$$

Take Spacing minimum value

$$S = 300 \text{ mm}$$

2.5 Design of Footing**To Find Loads:**

$$\text{Total load} = 383.91 \text{ kN} + [0.3 \times 0.4 \times 3 \times 25]$$
$$= 392.91 \text{ kN}$$

For 2 floor = 2×392.91

$$P = 785.82 \text{ kN}$$
$$P_u = 785.82 \times 1.5$$
$$= 1177.73 \sim 1200 \text{ kN}$$

To Find Area of Footing:

$$\text{SBC} = 300 \text{ kN/m}^2$$
$$\text{Area of footing} = 1200 / 300$$
$$= 4 \text{ m}^2$$

To Find Size of Footing:

$$4x \times 3x = 4$$
$$x^2 = 0.33$$
$$x = 0.577 \text{ m}$$
$$4x = 4 \times 0.577$$
$$= 2.3 \text{ m}$$
$$3x = 3 \times 0.577 = 1.73 \sim 1.75 \text{ m}$$

Size of footing = $2.3 \times 1.75 \text{ m}$

$$\text{Area} = 2.3 \times 1.75$$
$$= 4.025 \text{ m}^2$$

To Find Net Upward Soil Pressure:

Net upward soil pressure (q)

$$q = \text{load on footing} / A$$
$$= 1200 / 4.025$$
$$q = 298.13 \text{ kN/m}^2 < 300 \text{ kN/m}^2$$

To Find Moment:

Factored moment (Mud)

Mmax occur at the face to the column for design purpose

Consider only one overhang portion,

$$M_{ud} = 1.5$$

[Upward soil pressure x hatched x distance between C.G for end and Face to column]

$$= 1.5 [300 \times (0.95 \times 1.75) \times 0.475]$$
$$= 355 \text{ kN.m}$$

To Find Depth Upward for Moment:

Equate Mud to Mulimit

For M20 & Fe 415

From sp16 pg : 10, Table D

$$M_{ulimit} = 2.76 b d^2$$
$$355 \times 10^6 = 2.76 \times 1750 \times d^2$$
$$d^2 = 73573$$
$$d = 271.24 \text{ mm}$$
$$D = 271.24 + 50$$
$$D = 321.24 \text{ mm} \sim 400 \text{ mm}$$
$$d = 400 - 50$$
$$= 350 \text{ mm}$$
$$M_{ulimit} = 2.76 \times 1750 \times 350^2$$
$$= 591.67 \text{ kN.m}$$

Mulimit > Mud

It is under reinforced section

To Find Area of Main Reinforcement:

$$M_{ud} = 0.87 \times f_y \times A_{st} \times [d - f_y \times A_{st} / f_{ck} \times b]$$
$$355 \times 10^6 = 126367.5 A_{st} - 4.28 A_{st}^2$$
$$A_{st} = 3144.09 \text{ mm}^2$$

To Find Area of Distribution Reinforcement:

$$A_{stmin} = 0.12\% \text{ CSA}$$
$$= 0.12 / 100 \times 350 \times 1750$$
$$A_{stmin} = 735 \text{ mm}^2$$

To Find Spacing:

Use 20 mm dia of bar

$$S = a_{st}/A_{st} \times 1000$$

$$= (\pi/4 \times 20^2) / 3144 \times 1000$$

$$S = 170 \text{ mm}$$

Provide 20 mm dia bar @ 170 mm C/C in both direction

Check for Shear:
Check for One Way Shear:

$$V_u = 1.5 [q \times \text{hatched area}]$$

$$= 1.5 [300 \times 1.75 \times 0.55]$$

$$V_u = 433.12 \text{ kN}$$

$$\text{Resisting area for shear} = b \times d$$

$$= 1750 \times 550$$

$$= 962500 \text{ mm}^2$$

$$\tau_v = V_u / bd$$

$$= 433.12 \times 10^3 / 1750 \times 550$$

$$= 0.38 \text{ N/mm}^2$$

$$A_{st} = a_{st} / s \times 1750$$

$$= (\pi/4 \times 20^2) / 170 \times 1750$$

$$= 3233.99 \sim 3234 \text{ mm}^2$$

$$P_t = 100 A_{st} / bd$$

$$= 100 \times 3234 / (1750 \times 550)$$

$$P_t = 0.336$$

$$\tau_c = 0.40$$

$$k = 1$$

$$k \tau_c = 0.40$$

$$\tau_v < k \tau_c$$

$$0.38 < 0.40$$

Hence it is safe.

Check for Two Way Shear:
(Or)
Punching Shear:

Side length of critical plane = size of column + d/2 + d/2

$$\text{Short side} = 300 + 300/2 + 300/2$$

$$= 600 \text{ mm}$$

$$\text{Long side} = 400 + 400/2 + 400/2$$

$$= 800 \text{ mm}$$

Punching critical plane,

$$= 2(600) + (800)$$

$$= 2800 \text{ mm}$$

$$V_u = q \times \text{hatched area} \times 1.5$$

$$= 300 \times [(2.3 \times 1.75) - (0.6 \times 0.8)] \times 1.5$$

$$V_u = 1595.25 \text{ kN}$$

$$\tau_v = V_u / bd$$

$$= 1595 \times 10^3 / 2300 \times 400$$

$$= 1.04 \text{ N/mm}^2$$

Permissible Shear Stress:

$$\beta_c = \text{short side} / \text{long side}$$

$$= 300 / 400$$

$$\beta_c = 0.75$$

2.6 Design of Staircase

Design size = 2x3m

Height of each flight = 3/2 = 1.5m

Assume = 150mm (Rise) Tread = 300mm

Width of landing = 400mm

M20 @ Fe250

$$\text{No. of rise} = (1500 / 150) = 10$$

$$\text{No. of treads of each flight} = \text{no. of rise} - 1 = 9$$

Assume width of landing = 400mm

Live load = 3KN/m

To Find Effective Span:

$$l_e = (9 \times 300) + (400/2) + (400/2) + (230/2)$$

$$l_e = 3.125 \text{ m}$$

To Find Depth of Waist Slab:

$$\text{Depth of waist slab} = (\text{effective span} / 20)$$

$$= 3125 / 20 = 156.25 \text{ mm} \sim 160 \text{ mm}$$

$$D = 160 \text{ mm}$$

To Find Load Calculation:

$$\text{DL of slab (on slope)} = 0.16 \times 1 \times 25 = 4 \text{ KN/m}$$

$$\text{DL of slab on horizontal span} = W_s \sqrt{(R^2 + T^2)} / T$$

$$= 4 \sqrt{(0.15^2 + 0.3^2)} / 0.3 = 4.47 \text{ KN/m}$$

$$\text{DL of one step} = (1/2) \times \text{rise} \times \text{tread} = (1/2) \times 0.15 \times 0.3 = 0.563 \text{ KN/m}$$

$$\text{Load of steps per m length} = 0.563 \times 1 / (1000/300)$$

$$= 1.875 \text{ KN/m}$$

$$\text{Load due to floor finish} = 0.6 \text{ KN/m}$$

$$\text{Total DL} = 4.47 + 1.875 + 0.6 + 3 = 9.945 \text{ KN/m}$$

$$\text{Total ultimate load} = 9.945 \times 1.5 = 14.91 \text{ KN/m}$$

To Find Bending Moment:

Maximum bending moment @ center in ultimate BM

$$M_u = W_u \times l_{eff}^2 / 8 = 14.91 \times 3.125^2 / 8$$

$$= 18.20 \text{ KN/m}$$

Check for Depth:

$$\begin{aligned} \mu &= 0.149 \times f_{ck} \times b \times d^2 \\ &= 0.149 \times 15 \times 1000 \times d^2 \\ d_{req} &= 90 \text{ mm} \\ d_{req} &< d_{pro} \end{aligned}$$

To Find Ast for Main Reinforcement:

$$\begin{aligned} \mu &= 0.87 \times f_{yk} \times A_{st} \times d \left(\frac{1 - f_{yk} A_{st}}{f_{ck} \times b \times d} \right) \\ 18.20 \times 10^6 &= 29145 A_{st} - 3.62 A_{st}^2 \\ A_{st} &= 684.76 \text{ mm}^2 \end{aligned}$$

To Find Spacing:

Use 12mm ϕ
 $\text{Spacing} = (1000 \times a_{st} / A_{st}) = 165.15 \text{ mm} \sim 170 \text{ mm}$
 Provide 12mm ϕ @spacing 170 mm c/c

To Distribution Reinforcement:

$$\begin{aligned} A_{st \text{ min}} &= 0.15\% \times b \times d \\ &= (0.15/100) \times 1000 \times 160 \\ A_{st \text{ min}} &= 240 \text{ mm}^2 \\ \text{Spacing} &= (1000 \times a_{st} / A_{st}) \\ &= (1000 \times 78.53 / 240) \\ \text{Spacing} &= 300 \text{ mm} \end{aligned}$$

3. CONCLUSION

At the end of the site visit and experiencing real workspaces and the environment of construction, I realized that working at construction site is much more different and also more difficult, because of the weather conditions and the risks exist. This site visit gave me a chance to experience and learn what cannot be gained during lectures or tutorials. One of the first things that I have learnt is understanding the importance of safety which is a basic of construction, because of all dangers exist on site. Finally, this site visit helped for better understanding what I am going to face in future as a Quantity surveyor, and also giving me better understanding about construction to help me in my studying, especially for taking off in measurement. In overall, it was a great experience for me.

REFERENCES

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- [2] SP 16 Design Aids for reinforced concrete
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