

AN ADVANCED DROOP CONTROL METHOD FOR PROPORTIONAL REACTIVE POWER SHARING

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Abstract- For micro grid in islanded operation, due to the effects of mismatched line impedance, the reactive power could not be shared accurately with the conventional droop method. To improve the reactive power sharing accuracy, this paper provides an improved droop control method which mainly includes error reduction operation, self frequency operation and voltage recovery operation. The sharing accuracy is improved by the sharing error reduction operation, which is activated by the low-bandwidth synchronization signals. The error reduction operation will result in a decrease in output voltage amplitude. Therefore, the voltage recovery operation is proposed to compensate the decrease. The needed communication in this method is simple. Simulations results show that the improved droop controller can share load active and reactive power, enhance the power quality of the micro grid, and also have good dynamic performance.

Keywords: Micro grid, Droop control, Distributed Generation, reactive power sharing, self frequency control.

1. INTRODUCTION

Increased concerns about rising price of conventional energy (e.g. Fossil fuel) and environmental impacts are fast shifting the focus to the use of renewable and sustainable energy sources as fossil fuel reserves are going to vanish in the near future, so human beings will need to find alternative energy sources to avoid this disaster. The use of renewable energy sources is becoming popular along with fossil fuels depletion. The unpredictable and intermittent nature of renewable energy sources has kept them from integrating with the utility grid.

The popularity of distributed generation systems is growing faster from last few years because of their higher operating efficiency and low emission levels. Distributed generators make use of several micro sources for their operation like photovoltaic cells, batteries, micro

turbines and fuel cells. During peak load hours dgs provide peak generation when the energy cost is high and stand by generation during system outages. A micro grid is built up by combining a cluster of loads and parallel distributed generation systems in a certain local area. Micro grids have large power capacity and more control flexibility which accomplishes the reliability of the system as well as the requirement of power quality.

For sharing active and reactive power from multiple distributed generation units a voltage and frequency droop control methods are used. To maintain power control stability the total load demand sharing by distributed generation units should share equal load[1]. These distributed generation units are operated by inverters and DC storage units, where a number of parallel inverters are operated [2], [5]. To stabilize the system voltage and frequency. All the distributed generation units are highly responsible while sharing active and reactive power in an autonomous micro grid [4]. There are many techniques presented without control interconnection in [5], [9]. Conventionally, they are based on the frequency and voltage droop concept to achieve load sharing.

The reactive power sharing is sensitive to the impacts of mismatched feeder impedance while the real power sharing at steady state is always accurate [3]-[6]. The total loads must be properly shared by multiple distributed generation units in decentralized manner for an islanded micro grid [3], [5]. In many literatures the reactive power sharing accuracy in a simplified micro grid with two distributed generation (DG) units has been introduced [7]-[9]. For a networked micro grid configuration the reactive power sharing is more challenging. To reduce the reactive power sharing errors in micro grid system, some of improved methods have been introduced [2]-[8]. The control issues regarding reactive power sharing in networked micro grid is more challenging. To improve reactive power sharing and control in networked micro grid, this paper proposed a simple reactive power sharing compensation scheme.

Reactive power sharing errors are significantly reduced with this proposed method. After the compensation, the proposed droop controller will be automatically switched back to conventional droop controller. The proposed compensation method achieves accurate reactive power sharing at steady-state and is effective for micro grids.

In this paper, the advanced reactive power sharing method is proposed. The method improves the reactive power sharing by changing the voltage bias, which is activated by a sequence of synchronization events through the low-bandwidth communication network. It is a cost-effective and practical approach since only a lowbandwidth communication network is required. Simulation results are provided to verify the effectiveness and feasibility of the proposed reactive power sharing method[10].

2. DISTRIBUTED GENERATION

Distributed generations are small electric power generators. On the basis of the type and depth of penetration of distributed energy resource (DER) units, load characteristics and power quality constraints, and market participation strategies, the required control and operational strategies of a micro grid can be significantly different than those of the conventional power systems. DER units include both distributed generation (DG) and distributed storage (DS) units with different capacities and characteristics. At the low-voltage bus of the substation transformer the electrical connection point of the micro grid to the utility system, constitutes the micro grid point of common coupling (PCC) [2].

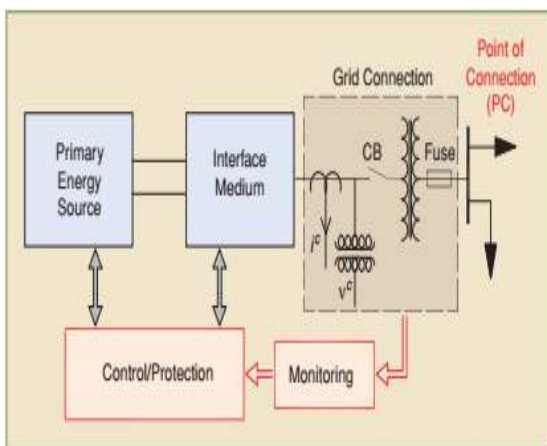


Fig.1: Basic Distributed Generation unit

3. MICRO GRID CONCEPT

It has been suggested that the solution to the reliability, accuracy and stability issues is to take advantage of micro grid technologies. The term –"micro grid" is quickly becoming a popular topic within the power community but it still remains vaguely defined [8].According to U.S. Department of Energy Micro grid Exchange Group defines a micro grid as a group of interconnected loads and distributed energy resources (DERs) within clearly defined that acts as a single controllable entity with respect to the grid.

Compared to use a single DG unit, micro grid could offer superior power management within the distribution networks. Moreover, the micro grid can operate in grid-connected mode or islanded mode and benefit both the utility and customers in economy –[12]. In an islanded mode, the load power in the micro grid should be properly shared by multiple DG units. Usually, the droop control method which mimics the behavior of a synchronous generator in traditional power system is adopted, which does not need the use of critical communications [13]–[18],

The accurate active power sharing is always simply achieved by the droop control method easily. However, due to effects of mismatched feeder impedance between the DGs and loads, the reactive power will not be shared accurately. In extreme situations, it can even result in severe circulating reactive power and stability problems [14].

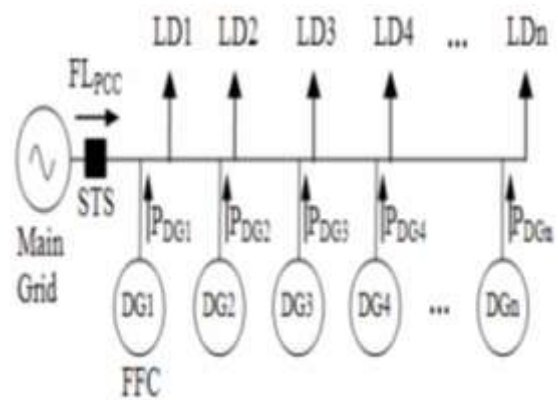


Fig 2 Architecture of micro grid

The Fig.2 shows the simplified diagram of grid connected micro grid which comprises of multiple DGs

3.1 Modes of operation of a micro grid:

A micro grid is connected to the utility grid through a bidirectional power converter that continuously monitors both sides and manages power flow between them [12-14]. If there is a fault in the utility grid, the power converter will disconnect the micro grid from the grid, creating an islanded energy system. Concluding, there are two operation modes for a micro grid:

A. Grid Connected Mode:

In the grid-connected operation mode, the grid-tied power converter has control over the DC link voltage level. If the output sum of the power of the distributed generation systems is sufficient to charge the storage devices, any excessive power is supplied to the utility grid.

B. Islanded Mode:

When a DC micro grid must be separated from the utility grid and switch to the islanded mode, the grid-tied power converter releases control of the DC link voltage level, and one of the converters in the micro grid must take over that control. A smooth transfer between grid-connected and islanded mode is essential for the reliability of a micro grid. When grid fault occurs, in order to protect the power electronic devices and some sensitive loads, the STS disconnects the micro grid from the grid.

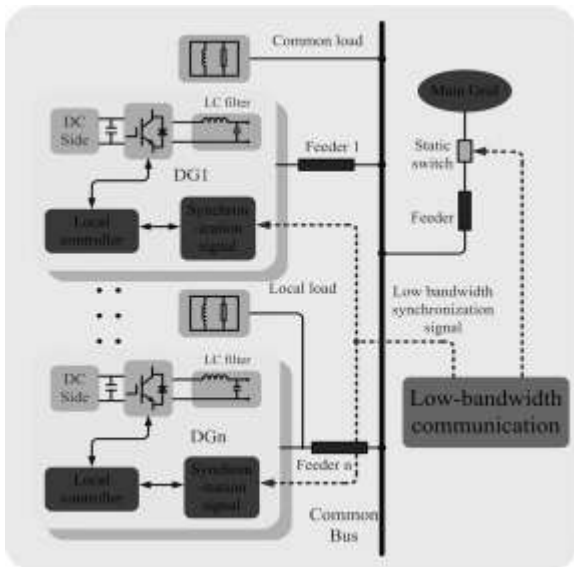


Fig 3 Illustration of the ac micro grid configuration

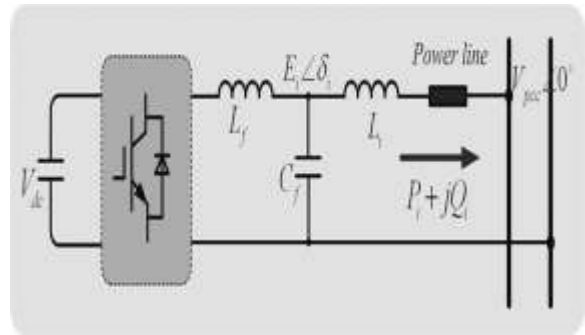


Fig 4 Model of a DG unit

4. PROPOSED DROOP CONTROL METHOD

The proposed control scheme for the *i*th DG unit is shown in Fig. 5, where the subscript *i* refers to the index of the DG; $P_{i,dis}$ and $Q_{i,dis}$ are the dispatched values of the active and the reactive power, respectively, from the CC; P_i and Q_i are the active and the reactive output powers of the DG, respectively; f_{nom} and V_{nom} are the nominal frequency and the voltage, respectively; $f_{i,ref}$ and $V_{i,ref}$ are the reference frequency and the voltage, respectively; f_i is the output frequency of the DG; $v_{abc,ref}$ is the three-phase voltage reference input to the voltage source; *a* and *b* are the nodes of the switch; m_i and n_i are the droop coefficients of frequency droop and voltage droop, respectively; and k_f and k_c are the integral gains for the self-frequency recovery control and the compensation control, respectively.

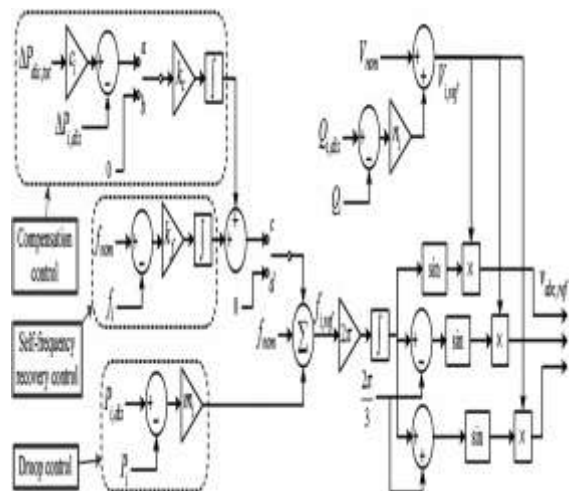


Fig.5 Proposed control scheme for distributed generation DG units.

The control method for the reactive power sharing uses conventional reactive power–voltage magnitude (Q–V) droop control. For this reason, the reference of the voltage magnitude

$V_{i,ref}$ is expressed as follows:

$$V_{i,ref} = V_{nom} + n_i (Q_{i,dis} - Q_i) \quad (1)$$

The reference voltage magnitude is determined from the deviation of the output reactive power from its dispatched value (which is usually zero with a unity power factor); therefore, the reference voltage magnitude is proportional to the Q–V droop coefficient n_i .

A. Droop Control

For basic control of active power sharing, the conventional P–f droop control was applied. The output frequency f_i can be expressed as

$$f_i = f_{nom} + m_i (P_{i,dis} - P_i) \quad (2)$$

The reference output frequency was determined from the deviation of the active power from the dispatched value (determined by the CC), which is proportional to the P–f droop coefficient m_i . Without self-frequency recovery control or compensation control, the frequency deviation from the nominal value can be determined using droop control only. With droop control, the exact load sharing among DG units is proportional to the droop coefficients. This process can be implemented by exchanging the same output frequency of each DG unit in the steady state; however, because the frequency will inevitably deviate from the nominal value and must be restored according to the grid code requirements, an additional control scheme for the frequency restoration is required.

B. Self-Frequency Recovery Control

The principal objective of self-frequency recovery control is to distribute the measures required to achieve frequency recovery among the DG units that participate in active power sharing using P–f droop control according to a predetermined ratio. The frequency restoration of the i th DG unit due to self-frequency recovery control can be expressed as

$$\Delta f_{i,res} = k_f \int (f_{nom} - f_i) dt \quad (3)$$

Where k_f is all the same value for every DG unit, which means that the burden of frequency restoration is shared equally among the DGs.

C. Compensation Control

To offset the errors in active and reactive power sharing caused by self frequency recovery control, a compensation control scheme was developed, as shown in Fig. 2. The main purpose of the compensation control is not to reduce transient frequency difference but to reduce the active power sharing error. Even if the transient frequency difference is small, the active power difference may be large since it depends on time of integration of the frequency difference and magnitude of line impedance. The output active power deviation of the i th DG is given by

$$\Delta P_{i,dis} = P_i - P_{i,dis} \quad (4)$$

The aggregate of all DG units can be found by summing the contributions from each unit; i.e.,

$$\Delta P_{dis,tot} = \sum_{i=1}^N \Delta P_{i,dis} \quad (5)$$

where N is the number of DG units participating in active power sharing. Because the objective of compensation control is to share the active power according to the ratio of the droop coefficients (i.e., m_1, \dots, m_N), $\Delta P_{dis,tot}$ should be distributed among the DG units considering the droop coefficients. Hence, the parameter c_i (see Fig. 2) was determined as follows:

$$c_i = \frac{1/m_i}{\sum_{j=1}^N (1/m_j)} \quad (6)$$

By multiplying c_i by $\Delta P_{dis,tot}$, we obtain the contribution of the i th DG unit to frequency recovery. Consequently, the compensation recovery control can be expressed as

$$\Delta f_{i,com} = k_c \int (c_i \Delta P_{dis,tot} - \Delta P_{i,dis}) dt \quad (7)$$

To communicate between the CC and DG units, and to assign $\Delta P_{dis,tot}$, a communications system is required, which may decrease system reliability. Ordinarily, the switch is connected to node b; in this state, the communications system is unnecessary and all DG units are controlled only using droop control and self-frequency control. If the micro grid operator decides to offset the active power sharing error, for all DG units, the switches are changed to node a by the CC. Using this switch, the communications system is utilized only when

the micro grid operator requires it or it can be automatically operated by periodical signal. Either way, the communication system failure does not significantly harm the system stability since it only concerns the active power sharing error.

By combining these three control schemes, the reference output frequency of the *i*th DG unit can be expressed as

$$f_{i,ref} = f_{nom} + m_i(P_{i,dis} - P_i) + k_f \int (f_{nom} - f_i) dt + k_c \int (c_i \Delta P_{dis,tot} - \Delta P_{i,dis}) dt. \quad (8)$$

To verify the effectiveness of the proposed control method for DG units, case studies were implemented. Table 1 lists the simulation parameters for all scenarios.

TABLE 1

ASSOCIATED PARAMETERS FOR POWER STAGE AND CONTROL OF THE DG UNIT

Parameters	Values	Parameters	Value
$L_f (mH)$	50	Nominal frequency $f_{nom} (Hz)$	50
$r_f (\Omega)$	0.01	P-f droop coefficient m (rad/wattsec)	1
$c_f (\mu F)$	20	Q-v droop coefficient n (v/var)	0.05
$L_{line1} (mH)$	1	Integral gain k_f	20
$L_{line2} (mH)$	1.5	Integral gain k_c	10

5. SIMULATION AND RESULTS

The proposed improved reactive power sharing strategy is verified with MATLAB/Simulink. In the simulations a micro grid with two DG systems, as shown in Fig. 6, is employed. The associated parameters for power stage and control of the DG unit are listed in Table 1. Also, in order to facilitate the observation of the reactive power sharing, the two DG units are designed with same power rating and different line impedances. The DG line current

and filter capacitor voltage are measured to calculate the real and reactive powers.

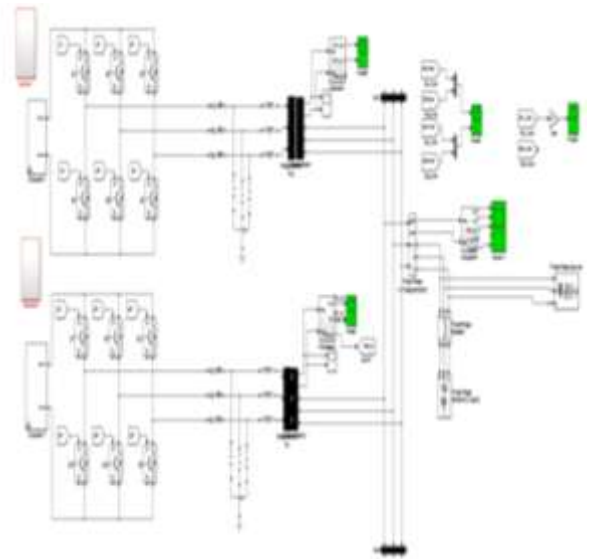


Fig 6. Configuration of the micro grid test system model

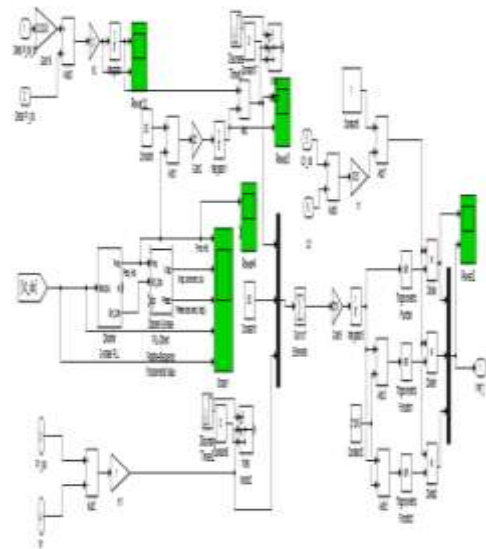


Fig. 7 Proposed control scheme for distributed generation DG unit

Case1: Power Sharing Accuracy Improvement:

Two identical DG units operate in parallel with the proposed voltage droop control. Fig.8 illustrates the reactive power sharing performance of the two DGs. Before $t = 0.05$ s, the sharing error reduction operation and voltage recovery operation are disabled. There exists an obvious reactive power sharing error due to the unequal voltage drops on the feeders. After $t = 0.05$ s, the reactive power sharing error reduction operation is performed, and it is clear that the reactive power sharing error converges to zero gradually. After $t = 0.1$ s, the voltage recovery operation is performed. It can be observed that the output reactive power increases but the reactive power sharing performance does not degrade. Fig. 8 shows the corresponding output voltages. It can be observed that the output voltages decrease during the sharing error reduction operation, while the voltage recovery operation ensures that DG output voltage amplitudes can restore back nearby to the rated value shows in fig.9. The whole process of adjustment can be done steadily in a relatively short period of time.

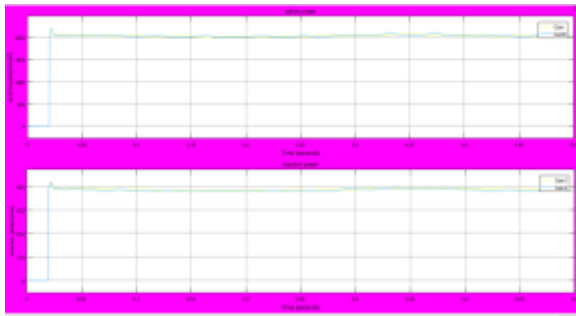


Fig. 8 . Simulated active and reactive power sharing performance in a networked micro grid (compensated is activated at 0.5 sec)



Fig. 9 Output voltage of DG1 And DG2

Case 2: Effect of the Communication Delay:

To test the sensitivity of the proposed improved droop control to the synchronized signal, a 0.02-s delay is intentionally added to the signal received by DG1 unit at $t = 0.25$ s and the simulation results are shown in Fig.10. Compared to the case 1 in Fig 8 and 9, a small disturbance appears in both the reactive and active power, while the voltage recovery operations are still able to ensure that the DG unit can deliver the expected reactive power. After $t = 0.25$ s, the active and reactive power sharing errors are almost zero. Therefore, the proposed reactive power sharing strategy is not sensitive to the communication delay. Then, it is illustrated that it is robust to some small communication delays.

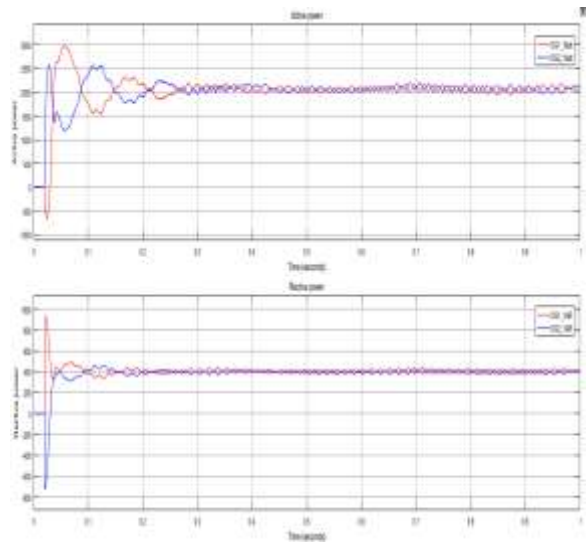


Fig.10 Simulated active and reactive power when 0.02-s time delay occurs in synchronization signal of DG1 unit.

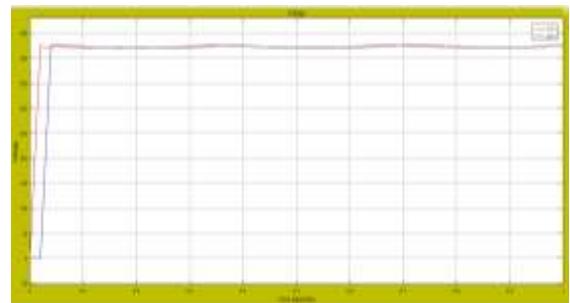


fig.11 Output voltage of DG1 And DG2 when 0.02-s time delay occurs in synchronization signal of DG1 unit.

Case 3: Effect of Load Change:

In order to test the effect of load change with the proposed method, the active load increases about 1.5kW and the reactive load increases about 0.5kVar at $t = 0.25$ s, and at $t = 0.25$ s the active load decreases about 1.5kW and the reactive load decreases about 0.5kVar. The corresponding simulation results are shown in Figs. 12 and 14. As can be seen, a large reactive power sharing deviation appears at $t = 0.25$ s and $t = 0.25$ s. However, the deviation becomes almost zero after a while. Fig.13 and 15 shows no change in output voltage.

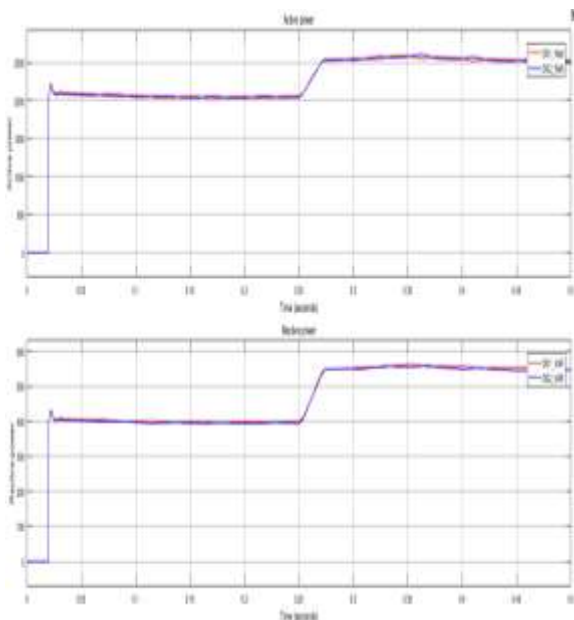


Fig.12.simulated active and reactive power when load is increased

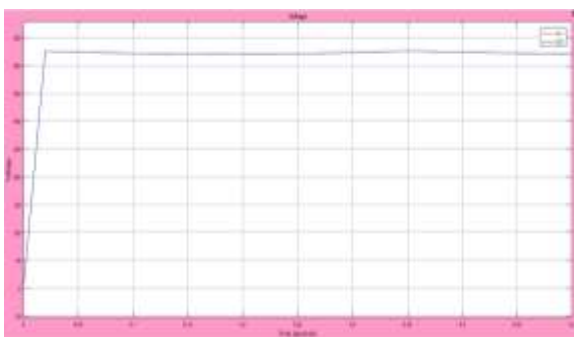


Fig.13. Output voltage of DG1 And DG2 when load is increased

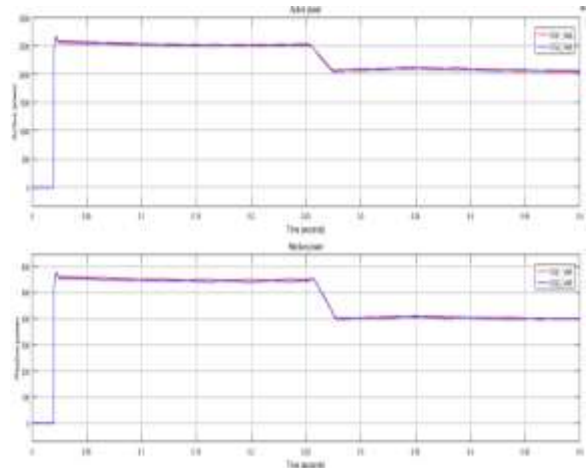


Fig 14. simulated active and reactive power when load is decreased

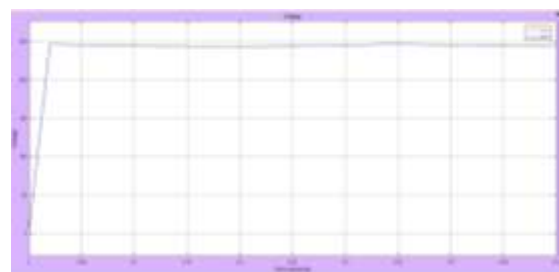


Fig.15 Output voltage of DG1 And DG2 when load is decreased

6. CONCLUSION AND FUTURE SCOPE

A control strategy to improve reactive power sharing in an islanded micro grid has been proposed in this paper. The proposed control strategy employs the communication network to exchange the information among the DG units to tune the adaptive virtual impedances in order to compensate the mismatch in feeder impedances. The advantage of the control strategy is that it does not require any information of the feeder impedances. It is also insensitive to time delays in the communication channels. Moreover, the proposed technique can also work well even when the transmission line is interrupted and the error of the power sharing is always low in the allowed limits. Simulation results shows that the frequency was restored almost immediately following frequency deviation using self-frequency control and also using compensation and droop control active and reactive power was shared accurately and effectiveness of the proposed method was verified.

In the future works, the proposed micro grid can be simulated with more number of DG sources and higher rating loads which can be installed for that configuration. four to five DG sources can be considered for this kind of study. Another area for the future work is the communications delay. Although a communications system is required only for a short duration (to implement compensation control), the communications delay may affect the control stability. Hence, determining the appropriate integral gain is desirable, which may avoid instabilities in the compensation control method.

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