

Enhancement of Power System Performance by Optimal Placement of Distributed Generation using Genetic Algorithms

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Abstract - In distribution network system, the DGs have many advantages which include decreasing power loss and improvement of voltage profile. These benefits can be achieved if DGs are optimally placed and sized in the system. This paper presents how to improve node voltage, power loss and MVA intake power in distributed network system due to DGs allocation strategy by using Genetic algorithm (GA). The main contribution of the research work has been to suggest to optimal placement of DGs and use of an optimal power flow based formulation to determine their settings. The suggested methods have been applied on 37-bus distribution systems.

Key Words: Distributed generations (DGs), Distribution networks, Different load models (DLMs), Genetic Algorithm (GA), Power system performances

1. Introduction

DG units are small generating plants connected directly to the distribution network or on the customer site of the meter. In the last decade, the penetration of renewable and non-renewable DG resources is increasing worldwide encouraged by national and international policies aiming to increase the share of renewable energy sources and highly efficient micro-combined heat and power units in order to reduce greenhouse gas emissions and alleviate global warming [1]. Electric utilities are now continuously searching upcoming new technologies to provide acceptable power quality and higher reliability to valuable customers. Non-conventional generation is growing more rapidly around the world due to its low size, low cost and less environmental impact with high potentiality. Investment in DG enhances environmental benefits particularly in combined heat and power applications [2].

1.1 Contribution of paper

In this paper, the different type of DGs with DLMs in distribution systems for enhancement of power system performances using GA. The comparisons of results are also presented in this paper.

1.2 Organization of paper

The organisation of paper are as follows: Section 2 discusses the mathematical problem formulation. Section 3 introduces the GA. Section 4 discusses the simulation results and

discussions. Section 5 introduces the conclusion of this paper and future scope of work.

2. Mathematical Problem Formulation

The mathematical models of DGs are explained in subsections 2.1-2.3, respectively [3]-[5].

2.1 General

For different types of load like as constant load models, industrial load models, residential load models, commercial load models, reference load models, the effect of different types of DGs i.e. DG-1, DG-2, DG-3, DG-4 an IEEE-38 bus distribution system is taken for simulation. The DG planning is to reduce the real power loss in distribution network. With some other power system performance indices like as reactive power loss, MVA capacity, voltage profile, and power flow reduction in the distribution network are used as objective function in the form of single or multi objective for optimization [3].

2.1.1 Reduce line loss

The mathematical formulation for loss minimization and objective function (f) is expressed as eq. (1).

$$f = \sum_{i_bus=1}^n P_{i_bus} \quad (1)$$

P_{i_bus} is the nodal injections of power in a network and n is total number of buses.

2.1.2 Increase capacity of DG

The optimal allocation of DG objective can maximize the DG capacity in eq. (2).

$$f = \sum_{i_bus=1}^n P_{DG i_bus} \quad (2)$$

$P_{DG i_bus}$ is the DG capacity of i_{th} bus.

2.1.3 Enhance socio-economic culture

Two objectives can be achieved first to enhance social welfare and second enhance of profit. social welfare is defined as difference between total benefit to consumers

minus total cost of production. The objective function associated with social welfare has been formulated as eq(3)-(4).

$$f = \sum_{i_bus=1}^n (B_{i_bus}(P_{Di_bus}) - C_{i_bus}(P_{Di_bus}) - C(P_{DG_{i_bus}})) \quad (3)$$

$$Pr\ of\ it_{i_bus} = \lambda_{i_bus} \times P_{DG_{i_bus}} - C(P_{DG_{i_bus}}) \quad (4)$$

$P_{DG_{i_bus}}$ is the DG Size at node i , $B_i(P_{Di})$ is quadratic benefit curve submitted by buyer (DISCO), minus quadratic bid curve submitted by seller (GENCO) $C_i(P_{Di})$, minus the quadratic cost function supplied by DG owner $C(P_{DG_i})$. λ_i denotes location margin price and $C(P_{DG_{i_bus}})$ is cost characteristic at node i .

2.1.4 Complex objectives

The complex objective aims are minimize the cost of setting up of DGs, DGs investment, DGs operational cost and total expenses toward compensating for system losses. Objective of this content to reduce the investment and operating costs of DGs, expenses toward purchasing the required extra power by the DISCO.

2.1.5 Load modeling

Planning of DGs for different load Models, a IEEE 38 distribution bus system is adopted. the line impedances, load data and line power limits are expressed in p.u. at the base voltage of 12.66 kV and base MVA of 10 MVA. In conventional load flow analysis the active and reactive power loads are assumed as constant power loads whereas in practice the loads may be voltage dependent. voltage dependent load model is a static load model that represents power relationship to the voltage as exponential equation and represented in eq. (5)-(6).

$$P_{i_bus} = P_{O_{i_bus}} \left(\frac{|V_{i_bus}|}{|V_{O_{i_bus}}|} \right)^{\alpha} \quad (5)$$

$$Q_{i_bus} = Q_{O_{i_bus}} \left(\frac{|V_{i_bus}|}{|V_{O_{i_bus}}|} \right)^{\beta} \quad (6)$$

Where, P_{i_bus} , Q_{i_bus} , $P_{O_{i_bus}}$, $Q_{O_{i_bus}}$, V_{i_bus} , and $V_{O_{i_bus}}$ are in per unit. Above eq. (5) and (6) neglect the frequency dependence of distribution system load. In practice, the load on each bus may be the composition of constant load models, industrial load models, residential load models, commercial load models, reference load models. the different load models at each bus is considered as described and represented in following form as eq. (7)-(8).

$$P_{i_bus} = W_{c_pi_bus} * P_{O_{i_bus}} \left(\frac{|V_{i_bus}|}{|V_{O_{i_bus}}|} \right)^{\alpha_c} + W_{i_pi_bus} * P_{O_{i_bus}} \left(\frac{|V_{i_bus}|}{|V_{O_{i_bus}}|} \right)^{\alpha_i} + W_{r_pi_bus} * P_{O_{i_bus}} \left(\frac{|V_{i_bus}|}{|V_{O_{i_bus}}|} \right)^{\alpha_r} + W_{m_pi_bus} * P_{O_{i_bus}} \left(\frac{|V_{i_bus}|}{|V_{O_{i_bus}}|} \right)^{\alpha_m} + W_{f_pi_bus} * P_{O_{i_bus}} \left(\frac{|V_{i_bus}|}{|V_{O_{i_bus}}|} \right)^{\alpha_f} \quad (7)$$

$$Q_{i_bus} = W_{c_qi_bus} * Q_{O_{i_bus}} \left(\frac{|V_{i_bus}|}{|V_{O_{i_bus}}|} \right)^{\beta_c} + W_{i_qi_bus} * Q_{O_{i_bus}} \left(\frac{|V_{i_bus}|}{|V_{O_{i_bus}}|} \right)^{\beta_i} + W_{r_qi_bus} * Q_{O_{i_bus}} \left(\frac{|V_{i_bus}|}{|V_{O_{i_bus}}|} \right)^{\beta_r} + W_{m_qi_bus} * Q_{O_{i_bus}} \left(\frac{|V_{i_bus}|}{|V_{O_{i_bus}}|} \right)^{\beta_m} + W_{f_qi_bus} * Q_{O_{i_bus}} \left(\frac{|V_{i_bus}|}{|V_{O_{i_bus}}|} \right)^{\beta_f} \quad (8)$$

Where, α_{c_i} and β_{c_i} are active and reactive exponents for constant load model α_{i_i} and β_{i_i} are active and reactive exponents for industrial load model; α_{r_i} and β_{r_i} are active and reactive exponents for residential load model; α_{m_i} and β_{m_i} are active and reactive exponents for commercial load model; α_{f_i} and β_{f_i} are active and reactive exponents for reference load model. $W_{c_pi_bus}$, $W_{i_pi_bus}$, $W_{r_pi_bus}$, $W_{m_pi_bus}$ and $W_{f_pi_bus}$ are the relevant factors for active constant, industrial, residential, commercial and reference Load models at bus i . $W_{c_qi_bus}$, $W_{i_qi_bus}$, $W_{r_qi_bus}$, $W_{m_qi_bus}$ and $W_{f_qi_bus}$ are the relevant factors for reactive constant, industrial, residential, commercial and reference Load models at bus i . The following condition must be satisfied for all buses except buses without load (BWL) (Bus 1 is slack bus and buses 34 to 38 are not having load) in eqs. (9)-(10).

$$W_{c_pi_bus} + W_{i_pi_bus} + W_{r_pi_bus} + W_{m_pi_bus} + W_{f_pi_bus} = 1 \quad (9)$$

for $i=1$ to N_B , but $i_bus \neq BWL$

$$W_{c_qi_bus} + W_{i_qi_bus} + W_{r_qi_bus} + W_{m_qi_bus} + W_{f_qi_bus} = 1 \quad (10)$$

for $i=1$ to N_B , but $i_bus \neq BWL$

2.2 DG modeling

The formulation of DGP problem is proposed on the basis of two objective functions such as real power loss and apparent power intake [10].

(i) Minimization of real power loss of the system

The objective function is total real power loss (P_L) in the system. The P_L in the system is represented by eq. (11).

$$P_L = \sum_{i,j_bus \in N_L} P_{ij_bus}^2 \frac{P_{ij_bus}^2 + Q_{ij_bus}^2}{|V_{i_bus}|^2} r_{ij_bus} \quad (11)$$

The P_L is function of all system bus voltage (V_{i_bus}), line resistances (r_{ij_bus}), α , and β . The total losses mainly depend on voltage profile.

(ii) Minimization of total MVA intake at main substation

The objective function is apparent power intake (S_{int}) at main substation. The P_{int} is the sum of P_D and P_L , and represented by eq. (12)-(13).

$$P_{int} = P_D + P_L \quad (12)$$

Similarly, the Q_{int} is the sum of Q_D and Q_L , and represented by eq. (13).

$$Q_{int} = Q_D + Q_L \quad (13)$$

Apparent power intake at main substation is expressed as equ. (14).

$$S_{int} = [(P_{int})^2 + (Q_{int})^2]^{1/2} \quad (14)$$

And apparent power requirement for distribution system is expressed as equ. (15).

$$S_{sys} = [(P_{int} + P_{DG})^2 + (Q_{int} + Q_{DG})^2]^{1/2} \quad (15)$$

It is observed that for a distribution system in eqs. (16)-(17).

$$\sum_{i_bus=1}^{N_B} P_{0i_bus} (|V_i|/|V_{0i_bus}|)^{\alpha} \gg P_L \quad (16)$$

$$\sum_{i_bus=1}^{N_B} Q_{0i_bus} (|V_i|/|V_{0i_bus}|)^{\beta} \gg Q_L \quad (17)$$

Thus the P_{int} and Q_{int} in eqs. (12)-(13) respectively are largely decided by the load exponents, α and β , not by P_L and Q_L .

$$V_{min} \leq |V_{i_bus}| \leq V_{max} \quad (18)$$

$$S_{i,j_bus} \leq CS_{i,j_bus}^{max} \quad (19)$$

$$P_{DG} \leq P_{int} \quad (20)$$

Where, $V_{min} = 0.95$ p.u., $V_{max} = 1.03$ p.u., CS_{i,j_bus}^{max} is the power capacity limit.

2.3 Power system performance indices [12]-[14]

(i) Real Power Intake Index (PI_Index)

The real power intake index is defined as:

$$PI_Index = \frac{PI_Index_{WDG}}{PI_Index_{WODG}} \times 100 \quad (21)$$

this index indicate reduction in P_{int} and more capacity release of substation. where, $P_{WODG} = 3.9039$

(ii) Reactive Power Loss Index (QI_Index)

The reactive power intake index is defined as:

$$QI_Index = \frac{QI_Index_{WDG}}{QI_Index_{WODG}} \times 100 \quad (22)$$

The lower values of this index indicate reduction in Q_{int} where, $Q_{WODG} = 2.4259$

(iii) Voltage Deviation Index (VD_Index)

The voltage deviation index is defined as:

$$VD_Index = \frac{VD_Index_{WDG}}{VD_Index_{WODG}} \times 100 \quad (23)$$

It is related to maximum voltage drop between each node and root node. The lower values of this index indicate better performance of the network. where, $V_{REF} = 1.0300$

(iv) Apparent Power Intake (Sint) Index (SI_Index)

The Apparent Power Intake Index is defined as:

$$SI_Index = \frac{SI_Index_{WDG}}{SI_Index_{WODG}} \times 100 \quad (24)$$

The lower values of this index indicate reduction in S_{int} , and more capacity release of substation. where, $S_{WODG} = 4.5962$

(v) Real Power Index (PL_Index)

The real power loss index is defined as:

$$PL_Index = \frac{PL_Index_{WDG}}{PL_Index_{WODG}} \times 100 \quad (25)$$

The lower value of this index indicates better benefits in terms of real power loss reduction accrued due to DG location & size. Where, $Min. Loss_{WODG} = 0.1889$

(vi) Real Power Penetration of DG (DG_P)

The ratio of the amount of DG active power injected into the network to the summation of active power with DG

$$\text{and without DG. } DG_P = \frac{P_{WDG}}{P_{WODG} + P_{WDG}} \times 100$$

(26)

(vii) Reactive Power Penetration of DG (DG_Q)

The ratio of the amount of DG reactive power injected into the network to the summation of reactive power with DG and without DG.

$$DG_Q = \frac{Q_{WDG}}{Q_{WODG} + Q_{WDG}} \times 100 \quad (27)$$

3. GA Implementation

A powerful class of optimization methods is the family of GA. The GA become particularly suitable for the problem posed here. GA based on power loss minimization and energy loss optimization technique is proposed for finding size and site for DG to place in power systems. If network structure is fixed, all branches between nodes are known and evaluation of the objective functions depends only on the size and location of DG units [3].

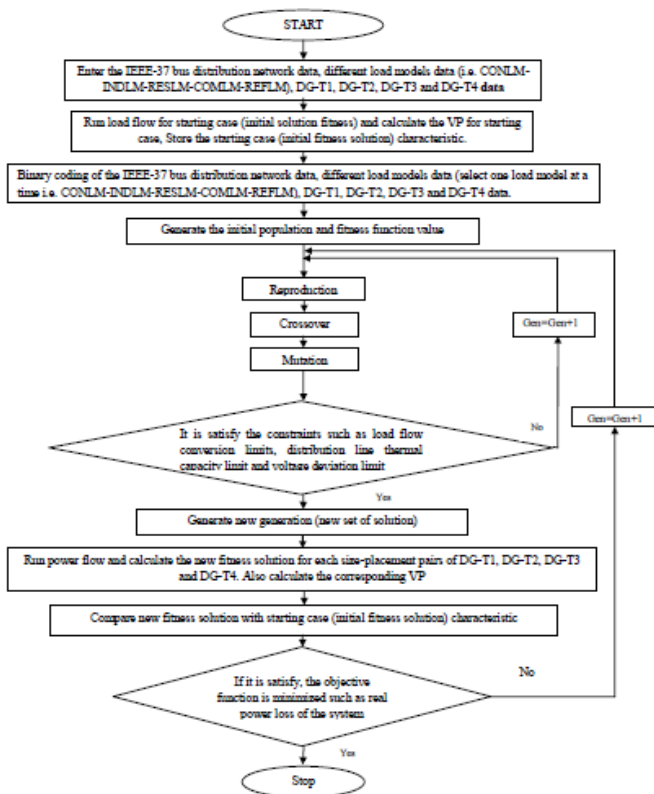


Fig. 1: The flowchart of GA for optimal placement and sizing of DG in distribution systems

GA that yields good results in many practical problems is composed of three operators:

- (i) **Crossover:** The individuals, randomly organized pairwise, have their space locations combined, in such a way that each former pair of individuals gives rise to a new pair.
- (ii) **Mutation:** Some individuals are randomly modified, in order to reach other points of the search space.
- (iii) **Selection:** The individuals, after mutation and crossover, are evaluated. They are chosen or not chosen for being inserted in the new population through a probabilistic rule that gives a greater probability of selection to the “better” individuals.

The advantages in using GA are that they require no knowledge or gradient information about the response

surface; they are resistant to becoming trapped in local optima and they can be employed for a wide variety of optimization problems.

4. Simulation Results and Discussions

4.1 General

The simulation results and discussions corresponding to DG-T1, DG-T2, DG-T3 and DG-T4 type operating at power factors 1.00, 0.85 leading, 0.00 and 0.85 lagging, respectively.

4.2 IEEE 37 Bus (38 Node) Test System and its Data

The IEEE 37 bus (38 nodes) test system and its data are given in Fig. 4 and Table 1, respectively.

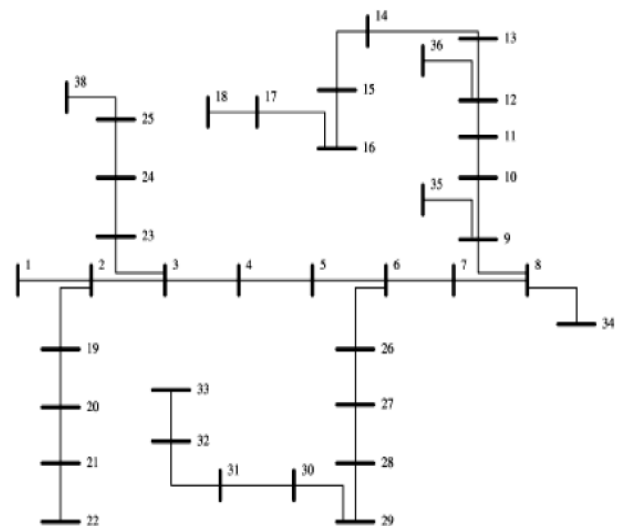


Fig. 2: IEEE 37 bus (38 node) test system [3]

Table 1: Line parameter and load data for 37 buses (38 nodes) test system [3]

F	T	Line impedance (p. u.)		L	S _L (p.u.)	Load on the bus (p. u.)	
		R	X			P	Q
1	2	0.0005 74	0.00029 3	1	4.60	0.1 0	0.0 6
2	3	0.0030 70	0.00156 4	6	4.10	0.0 9	0.0 4
3	4	0.0022 79	0.00116 1	1 1	2.90	0.1 2	0.0 8
4	5	0.0023 73	0.00120 9	1 2	2.90	0.0 6	0.0 3
5	6	0.0051 00	0.00440 2	1 3	2.90	0.0 6	0.0 2
6	7	0.0011 66	0.00385 3	2 2	1.50	0.2 0	0.1 0
7	8	0.0044	0.00146	2	1.05	0.2	0.1

		30	4	3		0	0
8	9	0.0064 13	0.00460 8	2 5	1.05	0.0 6	0.0 2
9	10	0.0065 01	0.00460 8	2 7	1.05	0.0 6	0.0 2
1 0	11	0.0012 24	0.00040 5	2 8	1.05	0.0 4	0.0 3
1 1	12	0.0023 31	0.00077 1	2 9	1.05	0.0 6	0.0 3
1 2	13	0.0091 41	0.00719 2	3 1	0.50	0.0 6	0.0 3
1 3	14	0.0033 72	0.00443 9	3 2	0.45	0.1 2	0.0 8
1 4	15	0.0036 80	0.00327 5	3 3	0.30	0.0 6	0.0 1
1 5	16	0.0046 47	0.00339 4	3 4	0.25	0.0 6	0.0 2
1 6	17	0.0080 26	0.01071 6	3 5	0.25	0.0 6	0.0 2
1 7	18	0.0045 38	0.00357 4	3 6	0.10	0.0 9	0.0 4
2	19	0.0010 21	0.00097 4	2	0.50	0.0 9	0.0 4
1 9	20	0.0093 66	0.00844 0	3	0.50	0.0 9	0.0 4
2 0	21	0.0025 50	0.00297 9	4	0.21	0.0 9	0.0 4
2 1	22	0.0044 14	0.00583 6	5	0.11	0.0 9	0.0 4
3	23	0.0028 09	0.00192 0	7	1.05	0.0 9	0.0 5
2 3	24	0.0055 92	0.00441 5	8	1.05	0.4 2	0.2 0
2 4	25	0.0055 79	0.00436 6	9	0.50	0.4 2	0.2 0
6	26	0.0012 64	0.00064 4	1 4	1.50	0.0 6	0.0 2
2 6	27	0.0017 70	0.00090 1	1 5	1.50	0.0 6	0.0 2
2 7	28	0.0065 94	0.00581 4	1 6	1.50	0.0 6	0.0 2
2 8	29	0.0050 07	0.00436 2	1 7	1.50	0.1 2	0.0 7
2 9	30	0.0031 60	0.00161 0	1 8	1.50	0.2 0	0.6 0
3 0	31	0.0060 67	0.00599 6	1 9	0.50	0.1 5	0.0 7
3 1	32	0.0019 33	0.00225 3	2 0	0.50	0.2 1	0.1 0
3 2	33	0.0021 23	0.00330 1	2 1	0.10	0.0 6	0.0 4
8	34	0.0124 53	0.01245 3	2 4	0.50	0.0 0	0.0 0
9	35	0.0124 53	0.01245 3	2 6	0.50	0.0 0	0.0 0
1 2	36	0.0124 53	0.01245 3	3 0	0.50	0.0 0	0.0 0
1 8	37	0.0031 13	0.00311 3	3 7	0.50	0.0 0	0.0 0
2 5	38	0.0031 13	0.00251 3	1 0	0.10	0.0 0	0.0 0

4.3 Real and reactive power exponential indexes for DLMs [9]

Table 2: Exponential indexes of DLMs

DLMs	Alpha	Beta
CONLM	0	0
INDLM	0.18	6.0
RESLM	0.92	4.04
COMLM	1.51	3.40
REFLM	0.91	1.0

4.4 Comparison of Results with Different type of DGs

The comparison of power system performance parameters such as Real power intake index (*PI_Index*), Reactive power intake index (*QI_Index*), Voltage deviation index (*VD_Index*), Apparent power intake index (*SI_Index*), Real power loss index (*PL_Index*), Real power penetration of DG (*DG_P*), Reactive power penetration of DG (*DG_Q*) with respect to DLMs such as constant, industrial, residential, commercial and reference load models are for DG-T1 type, DG-T2 type, DG-T3 type and DG-T4 type operating at different power factors such as 1.00, 0.85 leading, 0.00 and 0.85 lagging, respectively are shown in Fig. 3-9.

Table 3: Comparison of simulation results of *PI_Index* for different types of DGs with DLMs

<i>PI_Index</i>	CONLM	INDLM	RESLM	COMLM	REFLM
DG-T1	47.66	23.88	21.21	40.63	46.32
DG-T2	37.07	17.94	15.57	36.04	35.21
DG-T3	49.51	28.23	25.58	43.21	49.15
DG-T4	48.68	25.33	23.40	41.71	47.64

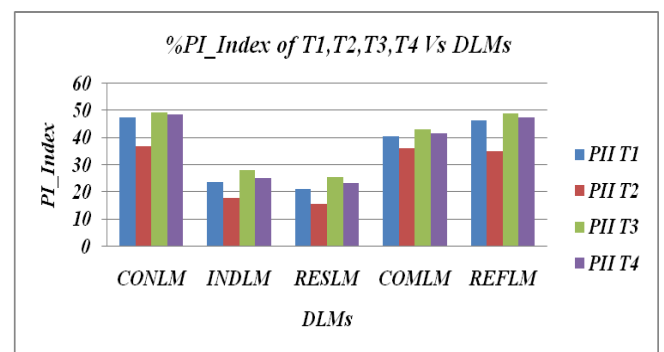


Fig. 3: *PI_Index* with DLMs

Table 4: Comparison of simulation results of *QI_Index* for different types of DGs with DLMs

<i>QI_Ind ex</i>	CONLM	INDLM	RESLM	COMLM	REFLM
DG-T1	45.21	21.38	20.12	38.69	44.23
DG-T2	36.95	17.88	15.53	35.93	35.10

DG-T3	48.40	25.58	30.40	41.84	48.69
DG-T4	47.53	23.18	25.34	39.60	46.52

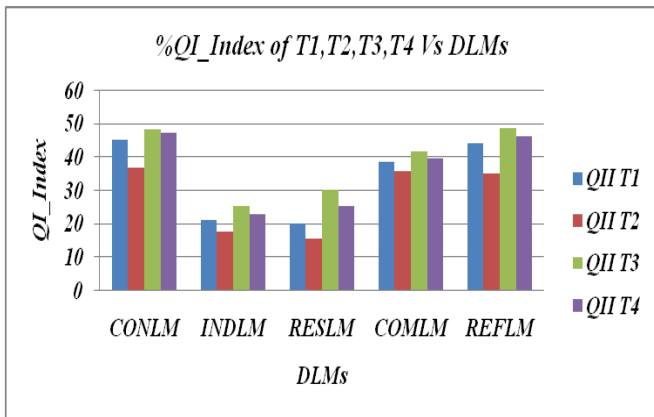


Fig. 4: QI_Index with DLMs

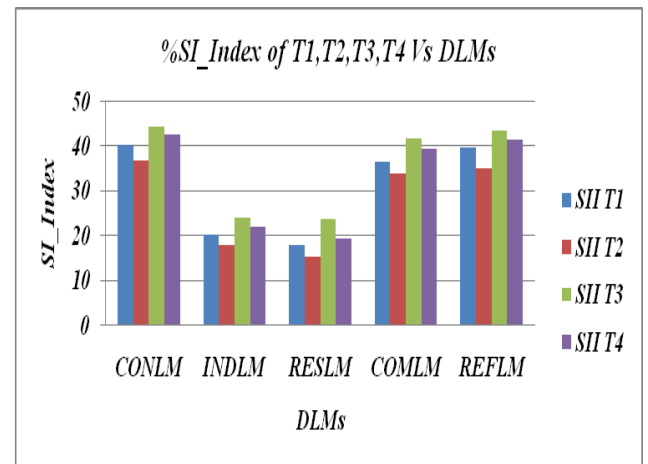


Fig. 6: SI_Index with DLMs

Table 5: Comparison of simulation results of VD_Index for different types of DGs with DLMs

VD_Index	CONLM	INDLM	RESLM	COMLM	REFLM
DG-T1	8.13	7.60	7.59	7.75	7.82
DG-T2	7.78	7.59	7.56	7.52	7.66
DG-T3	8.32	7.75	7.62	7.82	7.94
DG-T4	8.23	7.68	7.60	7.78	7.88

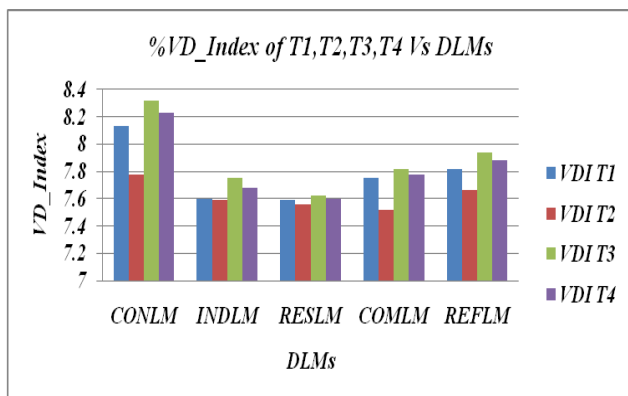


Fig. 5: VD_Index with DLMs

Table 7: Comparison of simulation results of PL_Index for different types of DGs with DLMs

PL_Index	CONLM	INDLM	RESLM	COMLM	REFLM
DG-T1	53.66	55.05	62.99	66.34	53.89
DG-T2	43.67	51.03	54.57	65.96	44.20
DG-T3	69.08	69.66	68.34	69.50	68.81
DG-T4	55.97	57.31	63.50	67.64	55.67

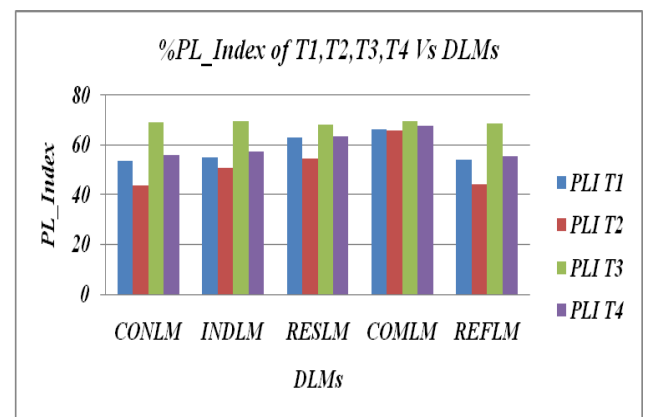


Fig. 7: PL_Index with DLMs

Table 6: Comparison of simulation results of SI_Index for different types of DGs with DLMs

SI_Index	CONLM	INDLM	RESLM	COMLM	REFLM
DG-T1	40.48	20.28	18.02	36.51	39.69
DG-T2	37.04	17.92	15.48	34.01	35.19
DG-T3	44.49	24.05	23.96	41.97	43.69
DG-T4	42.64	22.22	19.39	39.68	41.61

Table 8: Comparison of simulation results of DG_P for different types of DGs with DLMs

DG_P	CONLM	INDLM	RESLM	COMLM	REFLM
DG-T1	32.27	19.27	17.50	29.89	31.85
DG-T2	27.04	15.21	13.47	26.49	26.04
DG-T3	36.83	23.15	21.23	33.12	34.41
DG-T4	34.28	20.83	19.25	30.42	32.40

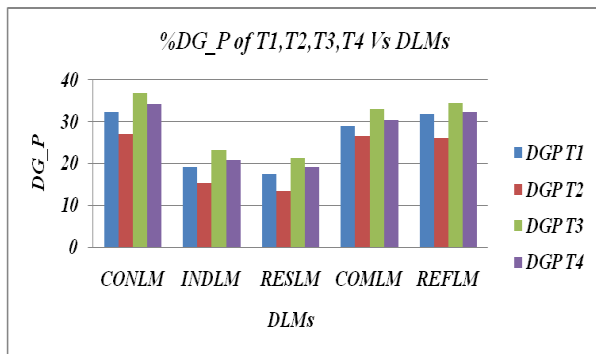


Fig. 8: DG_P with DLMs

Table 9: Comparison of simulation results of DG_Q for different types of DGs with DLMs

DG_Q	CONLM	INDLM	RESLM	COMLM	REFLM
DG-T1	28.23	17.29	21.21	26.21	27.21
DG-T2	26.98	15.17	13.44	24.43	25.98
DG-T3	34.69	31.31	31.22	31.45	32.74
DG-T4	32.22	26.79	26.20	28.36	29.33

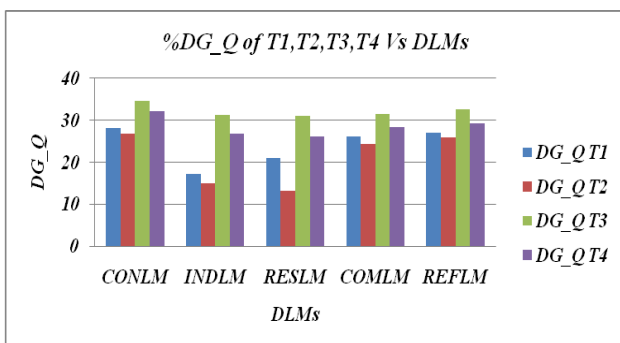


Fig. 9: DG_Q with DLMs

5. Conclusions

In this work different load model such as constant, industrial, residential, commercial and reference load models, at every bus for different type of DG such as DG-T1, DG-T2, DG-T3, DG-T4 are considered. The DG planning based gives appropriate result. It is desirable to keep the DG Planning indices i.e. Real power intake index (*PI_Index*), Reactive power intake index (*QI_Index*), Voltage deviation index (*VD_Index*), Apparent power intake index (*SI_Index*), Real power loss index (*PL_Index*), Real Power Penetration of DG (*DG_P*), Reactive Power Penetration of DG (*DG_Q*) below the limits which are defined without DG conditions. Proper sizing and location of DG can reduce losses, reduce MVA intake power, improve voltage profile, increase the loadability of system and reduce the real and reactive power losses of the system. DG-T2 type shows the best result in all the types of DGs. DGs performance order of DG-T2 > DG-T1 > DG-T4 > DG-T3.

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