

# SIMULATION AND ANALYSIS OF SHUNT ACTIVE POWER FILTER

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**Abstract-**This paper proposes a fuzzy logic controller for dc link voltage regulation to enhance the performance of widely used active power filter control strategies, namely, *p-q* method. The dynamic performance of the systems are Evaluated under different supply conditions and compared with the performances of the working with PI controller. The effectiveness of the fuzzy logic controller, in terms of total harmonic distortion (THD) in supply current and regulation of dc-link voltage is validated.

**Keyword-** Shunt APF, *p-q* method, dc-link voltage regulation, PI controller, Fuzzy logic controller.

## I INTRODUCTION

Since the past few decades, there has been intensive increase in the use of power converters and switching devices, various nonlinear loads and equipment's which draw highly non-linear current from the source and thereby inject harmonics in the system. These harmonics are perilous and greatly pollute the power system. They degrade power quality by increasing total harmonic distortion (THD) and reactive power consumption and also by causing poor power factor, voltage flicker, bad voltage regulation, voltage sags and swells, unbalanced load etc.[1]-[3]. Harmonics also cause electromagnetic interference (EMI) in communication network present within certain proximity. Issues pertaining to power quality are increasing steeply, therefore, tackling these problem become an indispensable task for maintaining a good power system.

Power filters came up as a viable solution for providing clean-harmonic free power at consumer ends. Conventionally, passive L-C filters were employed for harmonics mitigation and capacitors for power factor improvement. But gradually they got replaced by active power filters (APFs) because they are associated with certain inherent disadvantages like bulky size, mistuning, instability, resonance with load impedance or utility impedance and lack of flexibility. APFs give dynamic and versatile solution to the problem of power quality.

Research on APF technology boomed up and a large number of control techniques are being proposed and implemented. At present there is an appreciably large number of control methods used for power compensation by APFs.

This paper proposes a new fuzzy logic controller (FLC) for dc-link voltage regulation to enhance the performance of shunt APFs operating with *p-q* control method.

## II SYSTEM CONFIGURATION

Fig.1. Shows the system configuration of a power system compensated by shunt connected APF. The APF is a pulse width modulated (PWM) inverter and the non-linear load is composed of a three phase diode rectifier with R-L load. The PWM inverter is an IGBT based voltage source inverter (VSI). The values of system parameters are given in Appendix. The shunt-APF injects a compensating current which is an exact opposite of the distortion produced by the load to the line current, thus, nullifying the distortion. The amount of compensating power injected by the filter is controlled with suitable method to get perfect compensation.

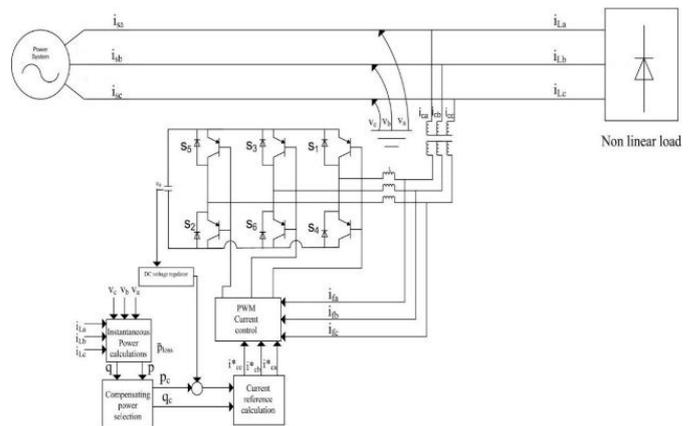


Fig. 1. System configuration of 3-phase compensated system

## III. CONTROL ALGORITHMS

Many methods to recognize and extract the harmonic voltage and current distortions which are classified as frequency analysis, time domain analysis and time frequency approach [9]. Instantaneous active and reactive power theory, (*p-q* theory) in time domain, can be used to identify the reference harmonic currents [9,10]. Offers the advantage to choosing the disturbance harmonics with precision, speed and ease implementation [10,11]. The first step of this method to transforming the three phase (a, b, c) voltages and currents to two-phase ( $\alpha, \beta$ ) using the direct conversion of Concordia. The principle adjustment of this method is to extract the fundamental component and harmonic removed component using low pass filters (LPF) [10,12,13]. The voltages and currents at the points of connections absorptive

by nonlinear load can be converted by the components of Concordia into:

$$\begin{bmatrix} v_0 \\ v_\alpha \\ v_\beta \end{bmatrix} = \sqrt{\frac{2}{3}} \begin{bmatrix} 1/\sqrt{2} & 1/\sqrt{2} & 1/\sqrt{2} \\ 1 & -1/2 & -1/2 \\ 0 & \sqrt{3}/2 & -\sqrt{3}/2 \end{bmatrix} \begin{bmatrix} v_a \\ v_b \\ v_c \end{bmatrix}$$

$$\begin{bmatrix} i_0 \\ i_\alpha \\ i_\beta \end{bmatrix} = \sqrt{\frac{2}{3}} \begin{bmatrix} 1/\sqrt{2} & 1/\sqrt{2} & 1/\sqrt{2} \\ 1 & -1/2 & -1/2 \\ 0 & \sqrt{3}/2 & -\sqrt{3}/2 \end{bmatrix} \begin{bmatrix} i_a \\ i_b \\ i_c \end{bmatrix}$$

The instantaneous real and imaginary power can be expressed by the following system:

$$\begin{bmatrix} p_L \\ q_L \end{bmatrix} = \begin{bmatrix} v_\alpha & v_\beta \\ -v_\beta & v_\alpha \end{bmatrix} \begin{bmatrix} i_{L\alpha} \\ i_{L\beta} \end{bmatrix}$$

The instantaneous real and imaginary power can be Decomposed into two AC and DC parts. The DC part resulted from the fundamental current and voltage and the AC part resulted from the harmonics [10,14]:

$$p^* = p + \tilde{p}$$

$$q^* = q + \tilde{q}$$

The references currents are calculated by the following expression:

$$\begin{bmatrix} i_{Ca}^* \\ i_{Cb}^* \end{bmatrix} = \frac{1}{v_\alpha^2 + v_\beta^2} \begin{bmatrix} v_\alpha & v_\beta \\ v_\beta & -v_\alpha \end{bmatrix} \begin{bmatrix} p^* \\ q^* \end{bmatrix}$$

Inverse transforms,

$$\begin{bmatrix} i_{Ca}^* \\ i_{Cb}^* \\ i_{Cc}^* \end{bmatrix} = \sqrt{\frac{2}{3}} \begin{bmatrix} 1 & 0 \\ -1/2 & \sqrt{3}/2 \\ -1/2 & -\sqrt{3}/2 \end{bmatrix} \begin{bmatrix} v_\alpha & v_\beta \\ v_\beta & -v_\alpha \end{bmatrix} \begin{bmatrix} p^* \\ q^* \end{bmatrix}$$

#### IV. HYSTERESIS BAND CURRENT TECHNIQUE

Hysteresis band current control does not need any information about the system parameters but has the disadvantage of uncontrolled switching frequency. The instantaneous value of the error can be calculated by subtracting from the identify reference harmonic currents ( $i_{ref}$ ) obtained by using diagram bloc of (p-q theory), and the injection harmonic currents ( $i_{inj}$ ) of (SAPF), subtraction between ( $i_{inj}$ ) and ( $i_{ref}$ ), introduced in hysteresis band current to generate the gate pulses [9,15,16], The hysteresis control law is given as fig. 2.

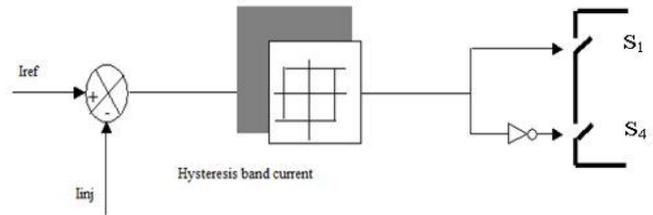


Fig. 2. Hysteresis band current control

#### IV. CONTROL OF DC VOLTAGE SOURCE OF (SAPF)

The advantage control of DC bus capacitor voltage source of (SAPF) arise suitable transit of supply power necessary added to power active fluctuate. The storage capacity C absorbs the power fluctuations caused by the compensation of the reactive power [17,18]. The normal conditioner, the real power supplied by the source should be equal to the real power demand of the load plus a small power to compensate the losses in the active filter [19]. Thus, the DC bus capacitor voltage can be kept at constant value and confirmed at a reference value. However, in the abnormal conditioner, In the presence of harmonics current, when the load changes, the real power balance between the source and the load will be disturbed. In this case, the real power poured most be compensated by the dc capacitor of inverter constructor of (SAPF). The changes of DC capacitor voltage from its reference most be regulate [19,20]. A fuzzy logic controller is applied to maintain the constant voltage across the capacitor by minimizing the error between the capacitor voltage and its reference voltage, the block diagram of a control is illustrated by the figure. 4.

To design the FLC, variables which should be chosen as the inputs to the controller are those that can represent the dynamic performance of the system that are to be controlled. The error (e) and the change of error (de) are taken as controller inputs, and the real power requirement for voltage regulation is taken as the output of the FLC. The input and output variables are represented by seven linguistic variables, namely, NL(Negative Large),NM(negative Medium),NS(Negative Small),ZE(Zero),

PS(Positive Small), PM(Positive Medium)and PL(Positive Large).Membership functions of the input and output variables are shown in fig. The fuzzy IF-THEN rules formed for controlling the DC voltage are given in Table-

Table I- Fuzzy Rule Base for Voltage Control

| Error (e) | Change in error(de) |    |    |    |    |    |    |
|-----------|---------------------|----|----|----|----|----|----|
|           | NL                  | NM | NS | ZE | PS | PM | PL |
| NL        | NL                  | NL | NL | NL | NM | NS | ZE |
| NM        | NL                  | NL | NL | NM | NS | ZE | PS |
| NS        | NL                  | NL | NM | NS | ZE | PS | PM |
| ZE        | NL                  | NM | NS | ZE | PS | PM | PL |
| PS        | NM                  | NS | ZE | PS | PM | PL | PL |
| PM        | NS                  | ZE | PS | PM | PL | PL | PL |
| PL        | NL                  | NM | NS | ZE | PS | PM | PL |

TABLE NO.1 MATLAB PARAMETER FOR SIMULATION

|                                  |             |
|----------------------------------|-------------|
| Supply Voltage and Frequency     | 100 V,50 Hz |
| Source Resistance and Inductance | 0.2Ω,1.5mH  |
| Filter Inductance                | 1mH         |
| DC Reference Voltage             | 300V        |
| DC Capacitor                     | 3000μF      |
| Load Resistance and Inductance   | 10Ω,100mH   |

### VII SIMULATION RESULTS

Simulations test is performed to confirm the validity of the proposed system. The (SAPF) was designed to compensate harmonics caused by nonlinear loads, the simulated results were obtained by using hysteresis band current and fuzzy logic controller was examined through Matlab/Simulink. The nonlinear load is a three-phase full-bridge diode rectifier supplying a RL load. The hysteresis band current is used to determine the switching time pulses of SAPF, the (p-q theory) is used to determine the three phases reference harmonic currents and the fuzzy logic controller is used to regulate DC bus capacitor voltage source of (SAPF). All spectrum harmonic analysis presented, should be limited in terms of total distortion harmonic (THD), and compared to the limit harmonic imposed by international standards [2].

Fig.4 show waveforms of the three phase source current currents and its spectrum harmonics analysis, without (SAPF), the THD is 20.45% before harmonic compensation. In this case, that is far the limit of the harmonic standard [2]. The reference harmonic currents identify using p-q algorithm as given in fig. 3.

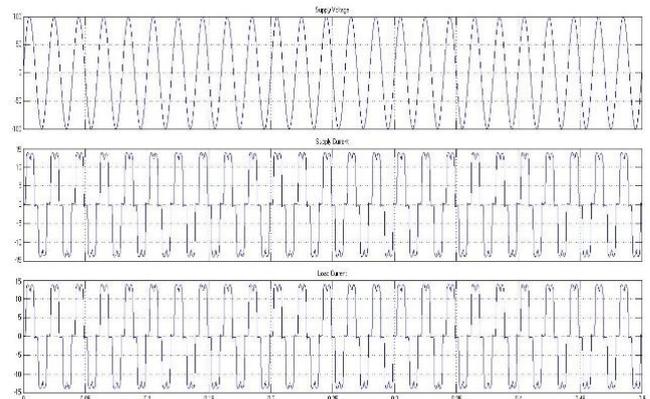
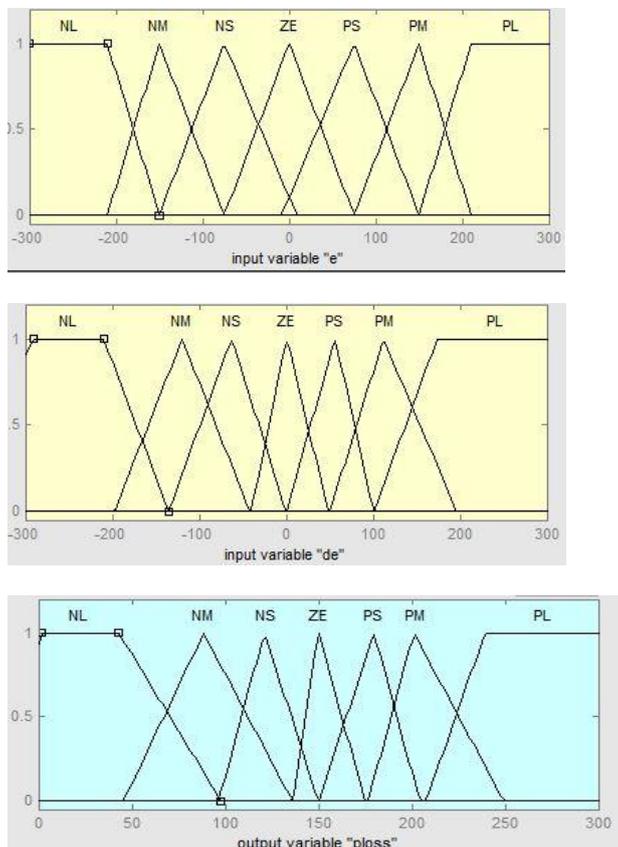


Fig 3 Waveform of Supply Voltage, Supply Current and Load Current without Filter.

The comparison between injection ( $i_{inj}$ ) and reference ( $i_{ref}$ ) currents of (SAPF) shown as fig. 9. We can be seen a better conformation and superposition with excellent properties. The fig.5,6, show waveforms of the three phase source current currents and its spectrum harmonics analysis, The THD decreases to at 2.54% using PI Controller and 1.61% using fuzzy controller before harmonic compensation, which is within the limit of the harmonic standard [2].

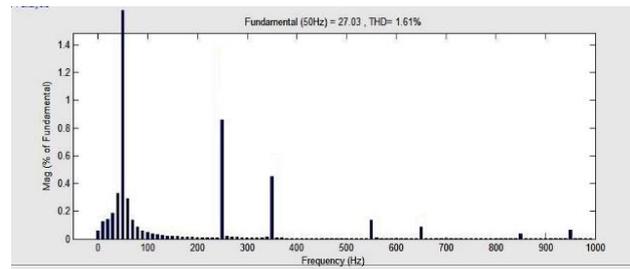


Fig 7. Supply Current THD with Filter using Fuzzy Controller

### VIII CONCLUSION

In this report the three phase three wire shunt active filter based on the instantaneous real and reactive power control strategy with PI controller have been analysed. It is found from the simulation results that shunt active power filter improves power quality of system by eliminating harmonics of non-linear load. The dc bus voltage has been maintained constant equal to the reference voltage by all PI and Fuzzy controllers. It has been found that these robust and nonlinear control proves to be better than conventional control. The THD of the source current is below 5% according to simulation result and it is in permissible limit of IEEE standard.

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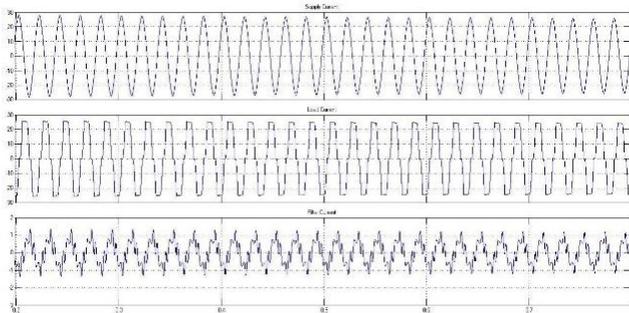


Fig 4. Waveform of Supply Current, Load Current and Filter Current with Filter using PI Controller

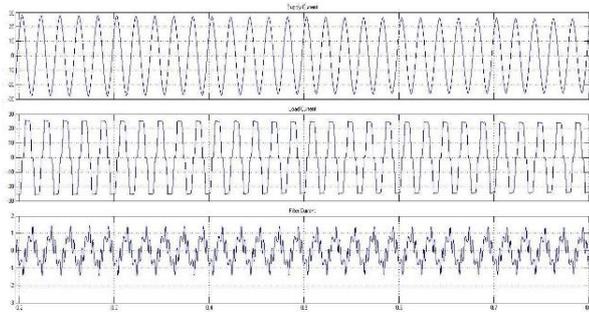


Fig 5. Waveform of Supply Current, Load Current and Filter Current with Filter using Fuzzy Controller.

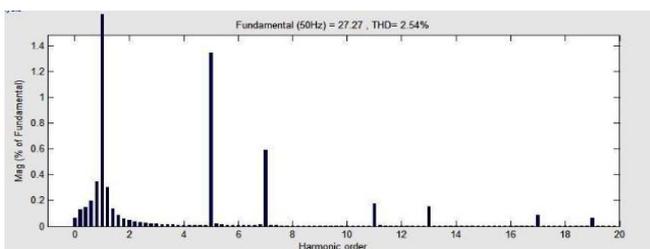


Fig 6. Supply Current THD with Filter using PI Controller

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